

**ISTC PROJECT #2267
&
SAD/YALINA-B Steering Committee
Meeting**

Dubna, Russia

July 12-13, 2004

S. Chigrinov

YALINA status and planning

ISTC B-070

***EXPERIMENTAL AND THEORETICAL RESEARCH ON TRANSMUTATION OF
LONG-LIVED FISSION PRODUCTS AND MINOR ACTINIDES IN
A SUBCRITICAL ASSEMBLY DRIVEN BY A NEUTRON GENERATOR***

Collaborators:

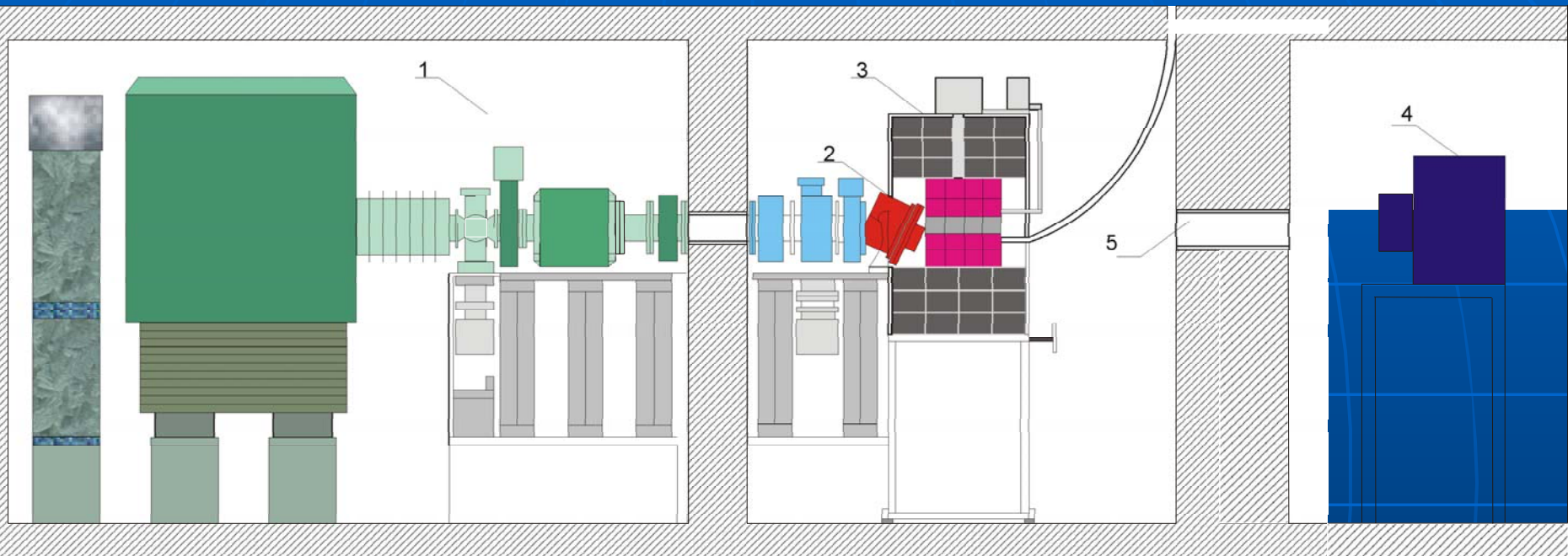
**W.Gudovski,
Royal Institute of Technology
Sweden**

**E. Gonzales,
Nuclear Fission Department
CIEMAT Spain**

**C. Broeders
Karlsruhe
Germany**

The main goals of the ISTC project :

- creation of the facility to investigate neutronic characteristics of the subcritical systems with thermal neutron spectrum, driven with external neutron sources (a Cf-252 spontaneous fission source, 2.5 MeV (D,D) and 14.1 MeV (D,t) neutron sources);
- measurements of the transmutation rates of fission products and minor actinides;
- investigation of kinetics of the sub-critical systems with external neutron sources;
- validation of the experimental techniques for, e.g., sub-criticality monitoring, neutron spectra measurement, etc;
- investigation of dynamics characteristics of the sub-critical systems with the external neutron sources with pulse mode of neutron generator operation.



1 - нейтронный генератор
 3 - подкритическая сборка
 5 - коллиматор

2 - $Ti-2H$ или $Ti-3H$ мишень
 4 - γ - спектрометр

- Accelerator H^+ and D^+
- Beam energy 100-250 КэВ
- Beam current 1 - 12 mA
- **Pulse duration** $(0.5-100)10^{-6}$ сек
- **Repetition rate** $(1-10\ 000)$ Hz
- **Spot size** ≈ 2.0 cm

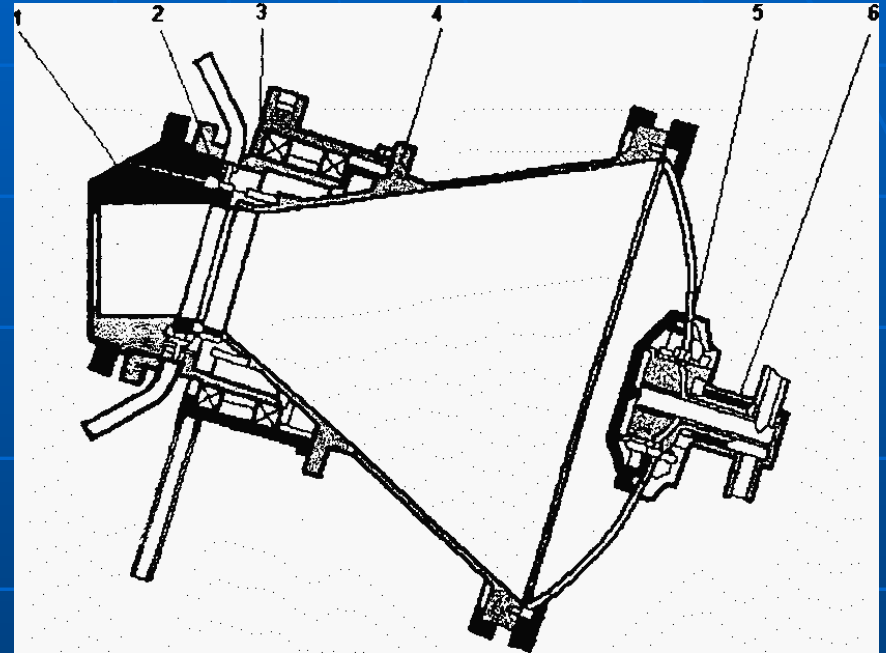
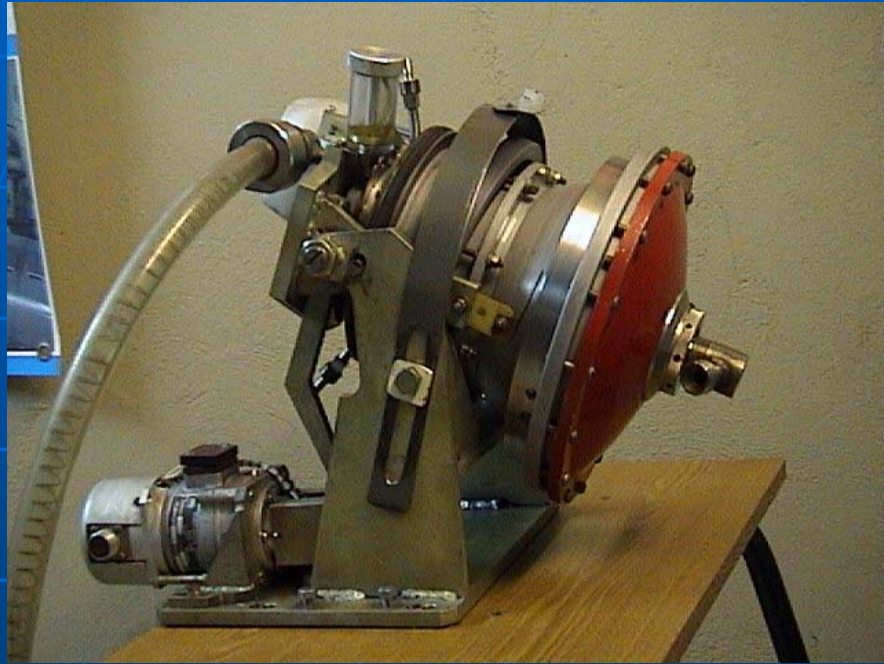
- **Ti3H target (230 mm):**
- Rotating speed, rpm 560
- Maximal yield of neutrons, n/s:
 $1.5-2.0 \cdot 10^{12}$
- Neutron energy 13-15 МэВ

- **TiD target (230 mm):**
- Maximal yield of neutrons, n/s:
 $2-3.0 \cdot 10^{10}$
- Neutron energy 2.5-3.0 МэВ



Neutron generator NG-12-1 ($D+^3H \rightarrow n+^4He$; $D+D \rightarrow n+^3He$)

TiH (TiD) targets characteristic



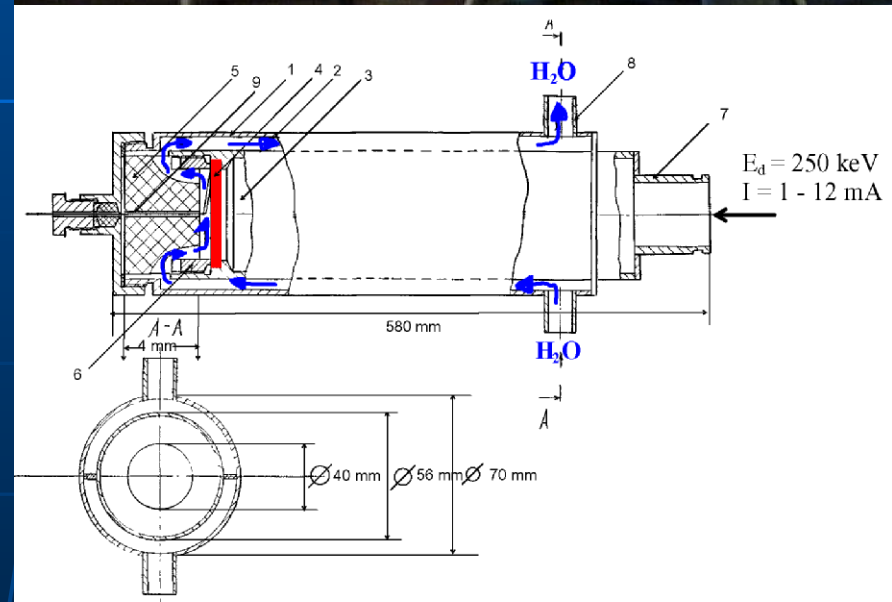
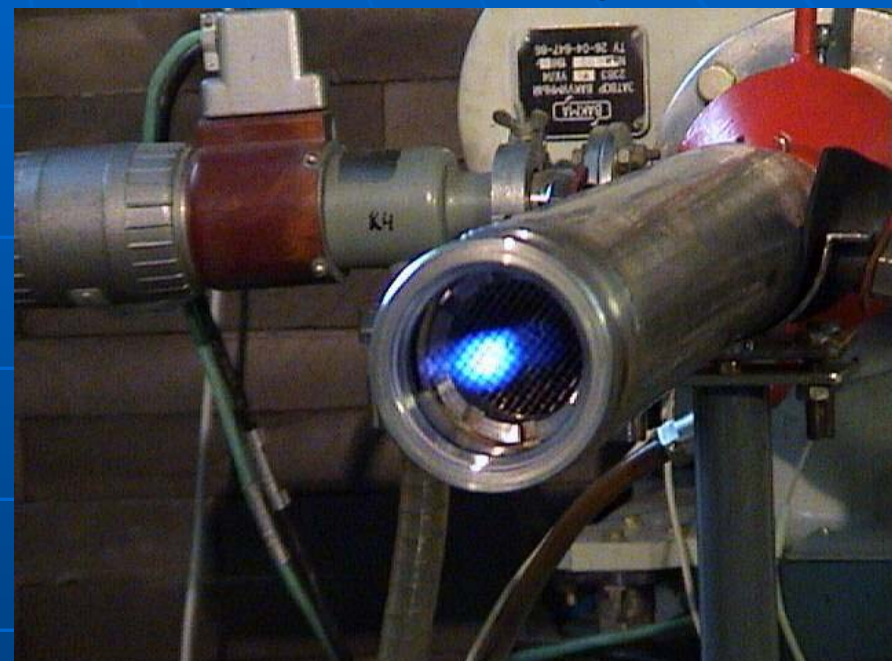
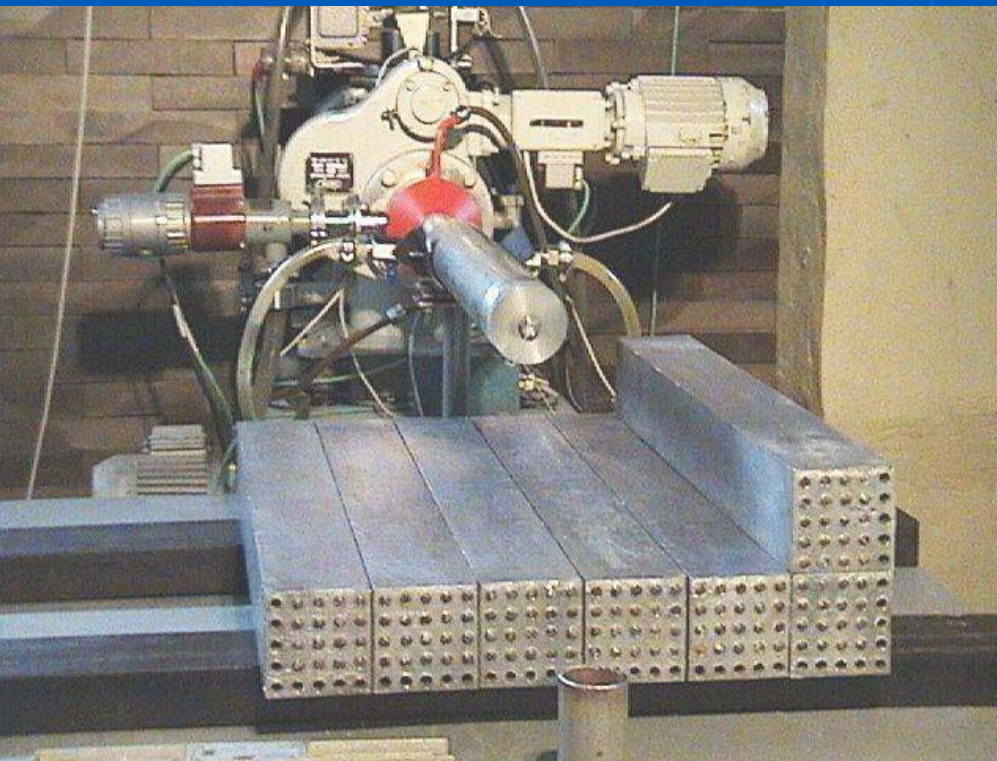
<u>Rotating speed</u>	<u>560 rpm</u>
<u>Target diameter</u>	<u>230 mm</u>
<u>Diameter of reaction space</u>	<u>100-200 mm</u>
<u>Tritium activity</u>	<u>0.53-0.75 MCi/kg</u>
<u>D/Ti (T/Ti) atomic ratio</u>	<u>≈ 1.5</u>

Target diameter

45 mm

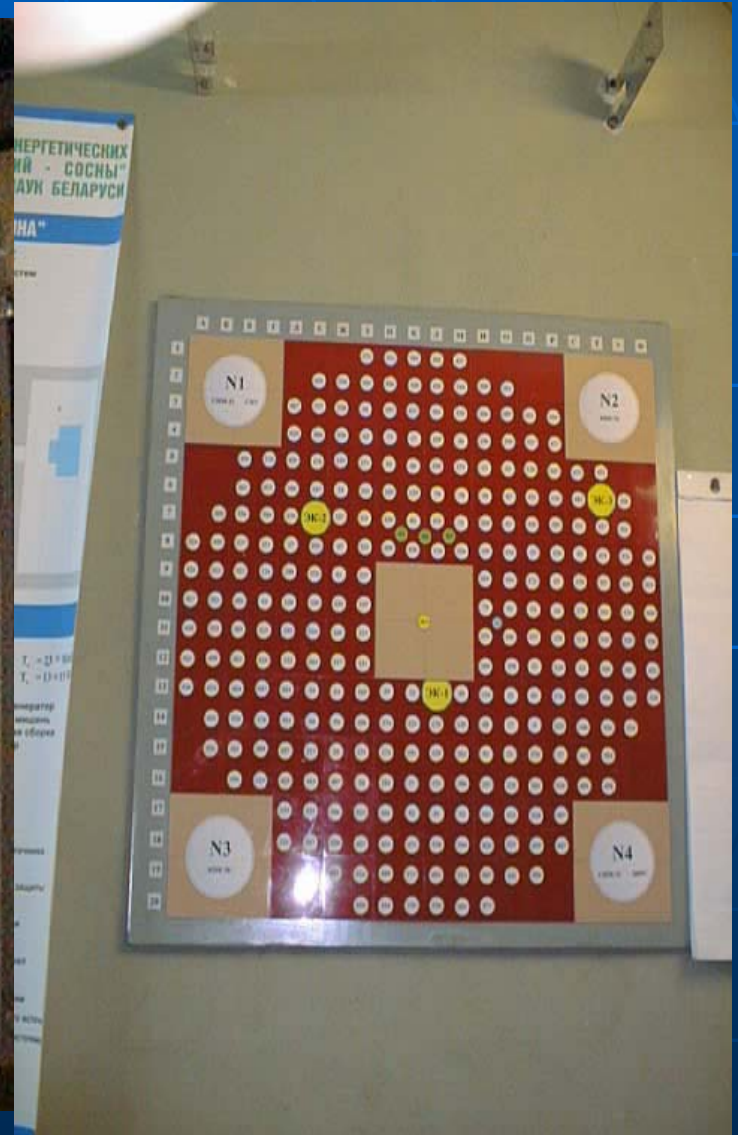
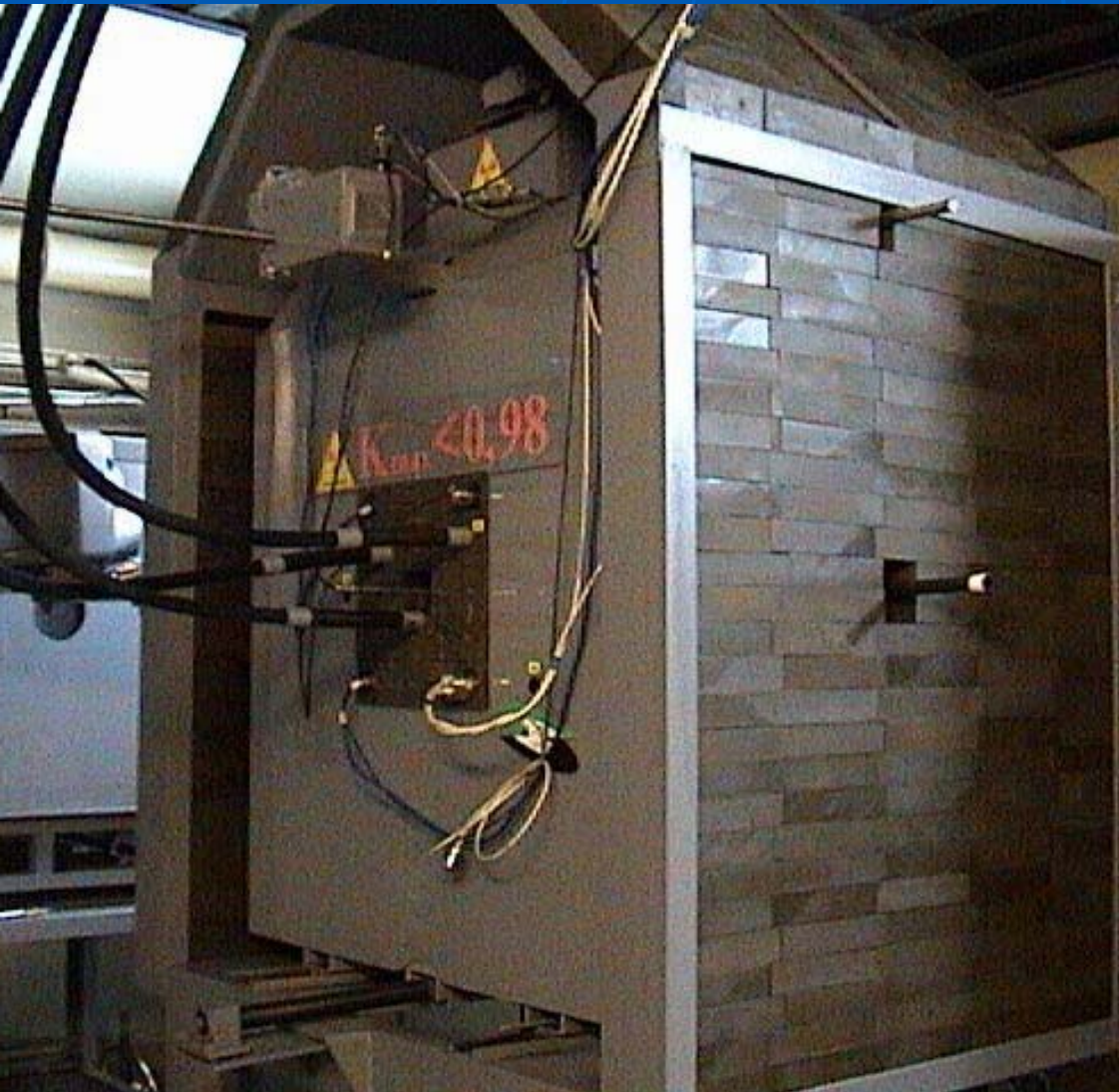


The NG-12-1 Deuteron guide (MM – L) for 45 mm diameter Ti₃H (TiD) targets



Subcritical assembly with thermal neutron spectrum

$K_{eff} = 0.98$ (Total mass of uranium - 21949.5 g)



Fission chambers without integral cable for in-core use

Type	Diameter nominal, mm	Detector length nominal, mm	Detect or length sensitive, mm	Isotope	Sensitivity to thermal neutrons		Sensitivity to fast neutrons $\text{cs}^{-1} / \text{n}\cdot\text{cm}^{-2}\cdot\text{s}^{-1}$	Sensitive square, cm^2	Sensitive layer, (mg· cm^{-2})	Filling gas
					Pulse mode ($\text{cs}^{-1} / \text{n}\cdot\text{cm}^{-2}\cdot\text{s}^{-1}$)	Current mode (A / $\text{n}\cdot\text{cm}^{-2}\cdot\text{s}^{-1}$)				
KNT-56	50	750	525	^{10}B	—	$4\cdot 10^{-13}$	—	—	—	BF_3
KNT-10	7	70	5	^{10}B	—	—	—	1	0,5	
KNT-2	7	70	10	^{232}Th	—	—	$6\cdot 10^{-7}$	2	5	98%Ar + 2%N ₂
KNT-5	7	70	5	^{235}U	$5\cdot 10^{-4}$	—	—	1	1	98%Ar + 2%N ₂
KNT-8	7	70	10	^{238}U	—	—	$2\cdot 10^{-6}$	2	5	98%Ar + 2%N ₂
KNT-31	32	235	200	^{235}U	0,25	—	—	500	1	98%Ar + 2%N ₂
KNT-54	50	242	220	^{235}U	0,5	—	—	1000	1	98%Ar + 2%N ₂
0.5 NHI/IK	10	62.5	10	He^3	0.5	-	-	-	-	He^3+Kr

2. He-3 detectors (10 mm diameter (NH10NM))

<i>Type</i>	<i>Effective length, mm</i>	<i>Neutron sensitivity, (c*s⁻¹/n*cm⁻²s⁻¹)</i>
0,5NKI/IK	10	0,5
12NK40/I	250	12

Technical characteristics of available equipment

1. Time analyzer TURBO MCS (ORTEC)

- Max counting rate 150 MHz;
- Channel width 5 ns – 65 535s;
- Pass length to 16 384 channels
- Memory capacity 16 777 215 counts/channel;
- Input amplitude from -5B to +5B;
- min input pulse width 3 ns.

3. Charge sensible amplifier for He-3 detectors (ACHNP97 and ACHNA98 types)

dead time – 0.8 μ s;
counting losses 3.1% at 40 000cps

4. 7820 ADS module –programming pulse amplifier- discriminator NIM standard

- **rise time – 20ns;**
- **resolving time – 50ns.**

5. Module NIM standard 7821 – 5th ports programming high-voltage power source - to +2000 B.

PROGRAMMABLE PULSE AMPLIFIER & DISCRIMINATOR NIM MODULE

FUEL CYCLE

7820

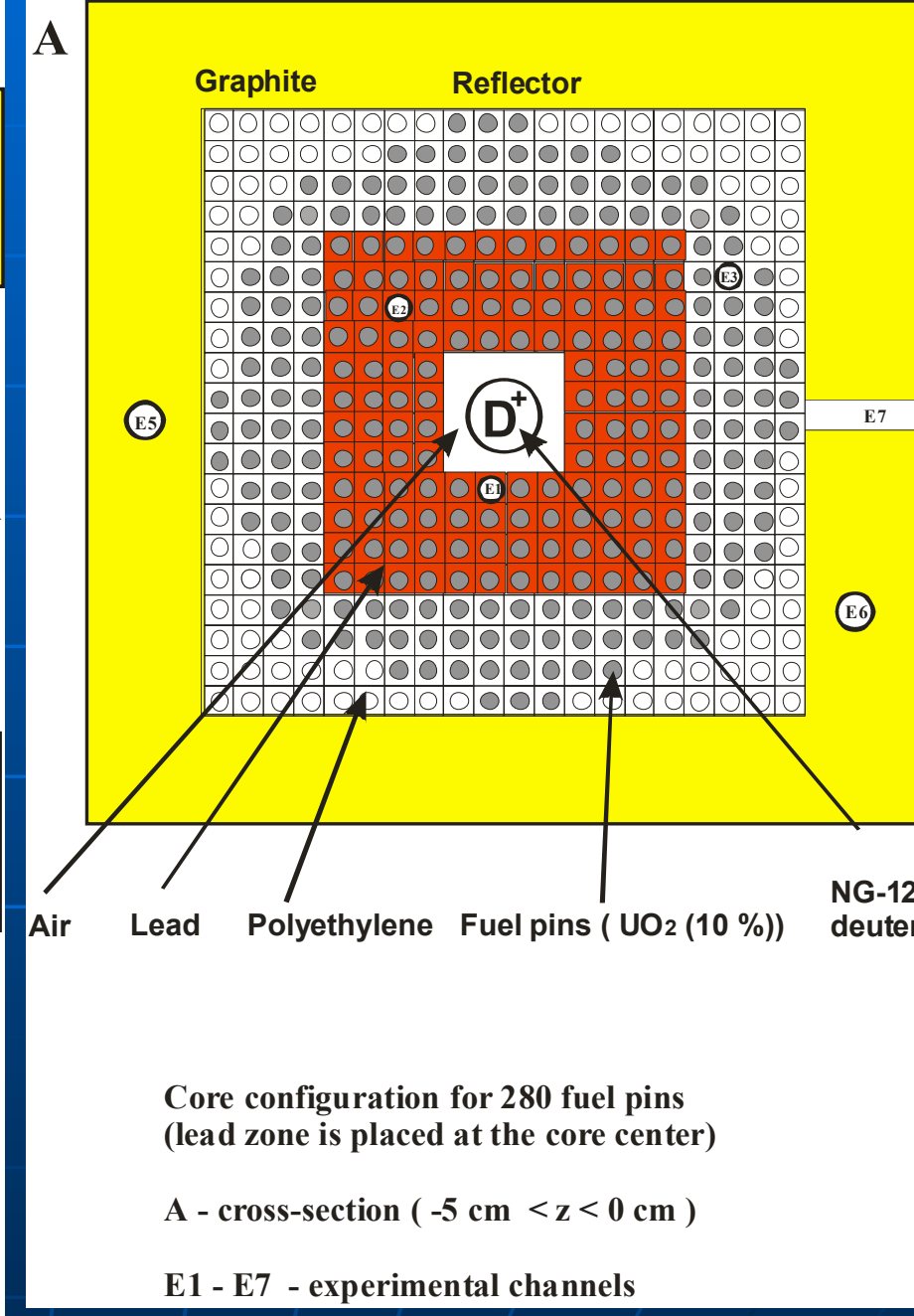
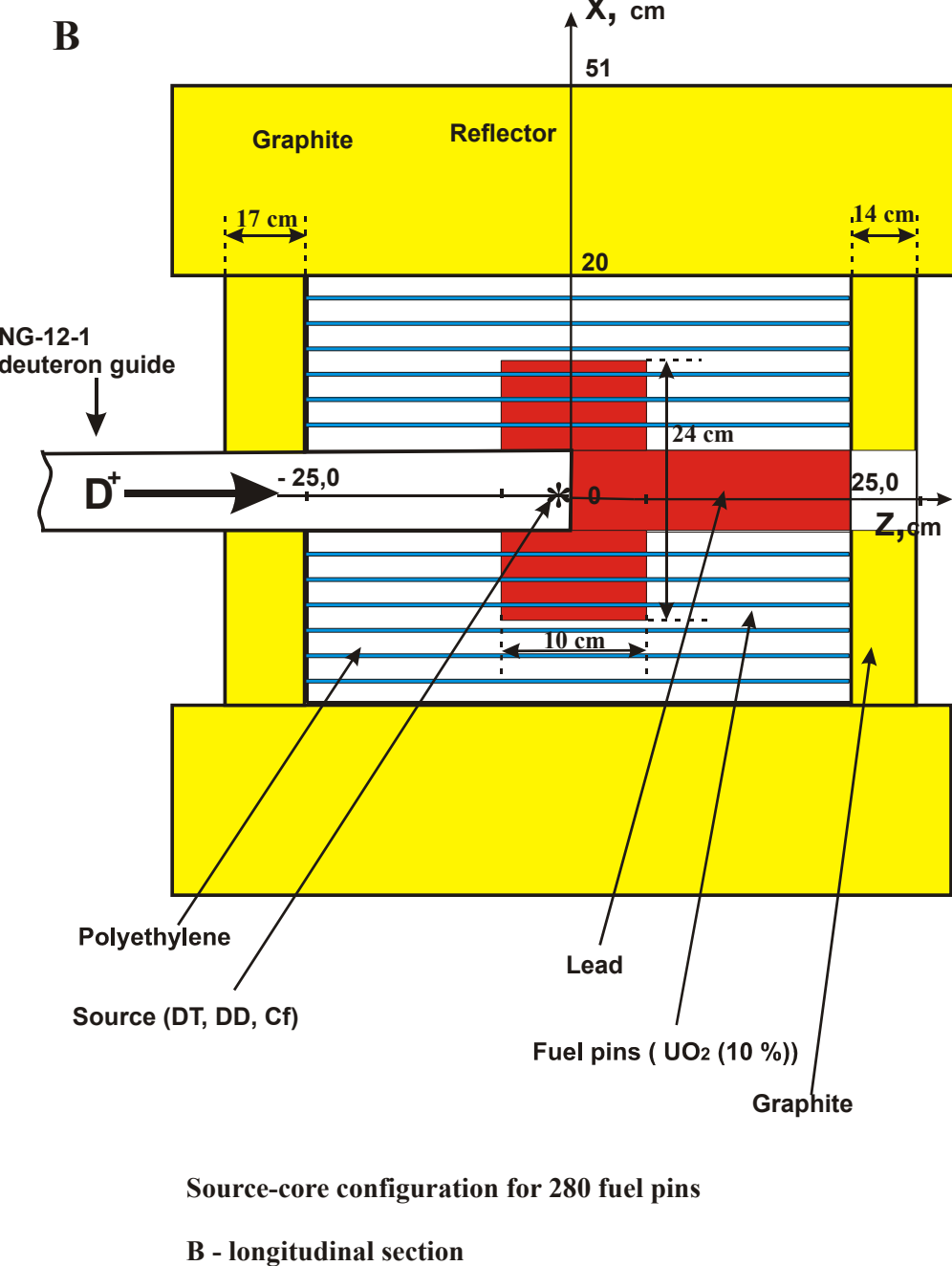
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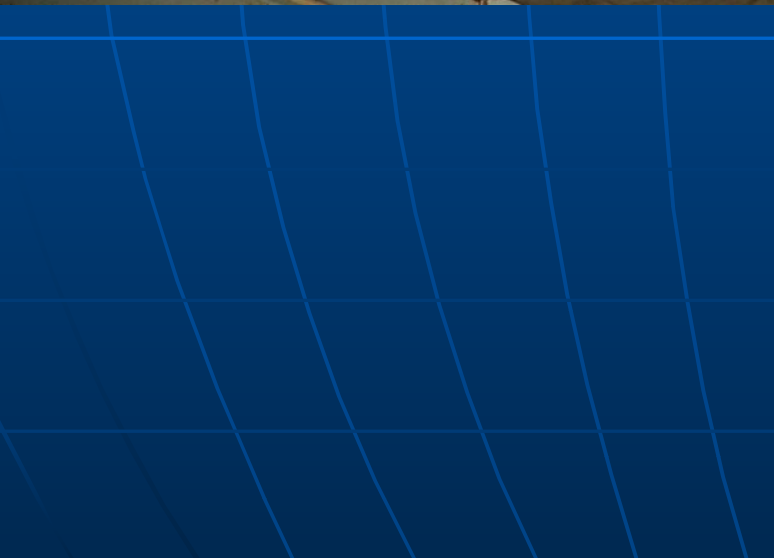
- **For all radiation pulse detectors (α , β , γ , X and neutrons)**
- **Perfectly adapted to neutron measurements with fission chamber or bore deposited counter (followup of reactor power or measurement of spent fuel)**
- **Fully programmable by PC computer via RS232, RS485 and Ethernet built-in interfaces**
- **Check-up of pre-defined values via the computer link**

- **High count rates up to $8 \cdot 10^6$ c/s**

- **Current collection operation allowing coaxial long distance connections without preamplifier up to 250 m**
- **Integrated TTL insulated outputs for external counting units**
- **Built-in test generator**
- **Connection to the ADC of an MCA for control purposes**

- Coaxial HPGe detector 80 % relative efficiency,
 - resolution (FWHM) –
 - 0.9 keV (122 keV), 1.8 keV (1332 keV).
- Low energy germanium detector (active area - 500 mm²),
 - resolution (FWHM) – 550 eV (122 keV).
 - Spectroscopy software GENIE-2000.
- MGA и MGAU software for multi group analysis of Uranium and Plutonium.
 - U-Pu Inspector Canberra Industries, Inc
 - standard tritium water samples;
 - the Np-237, Am-243 and I-129 samples ;
 - BF3 - chambers





SHORT- TERM EXPERIMENTAL PROGRAM

- 1.1. Measurement of multiplication factor of "new" (rearranged) core of the subcritical assembly (with lead zone in the core centre).
- 1.2. Measurements of spatial distribution of neutron flux density in the core (in experimental channels of the core and reflector).
- 1.3. Measurements of time dependence of neutron flux density inside experimental channels of subcritical assembly (in the core and the reflector) with pulse mode operation of neutron generator

II Kinetic measurement ($\Lambda, \rho, \alpha, \beta$)

- a) Source multiplication method (critical loading experiment);
- b) pulsed neutron method;
- c) noise analysis method (Feynman-alpha method)
- d) Systrand method (area method)
 $Ad/Ap = \beta/\rho; Y = A + B e^{-at}; \alpha = (\beta - \rho)/\Lambda; \beta = 7.37 \cdot 10^{-3}$
- e) Gozani, T. Nukleonik 4(1962), 348.
 $-\rho = f A/aB; f - \text{pulse repetition } (f \approx 54 \text{ Hz}); Y = A + B e^{-at}$
- f) Source jerk method

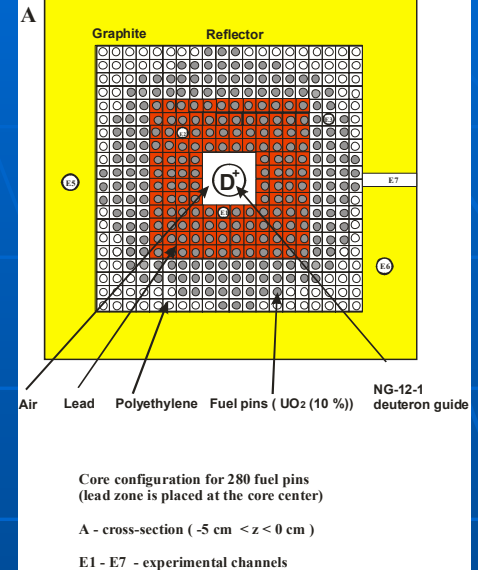
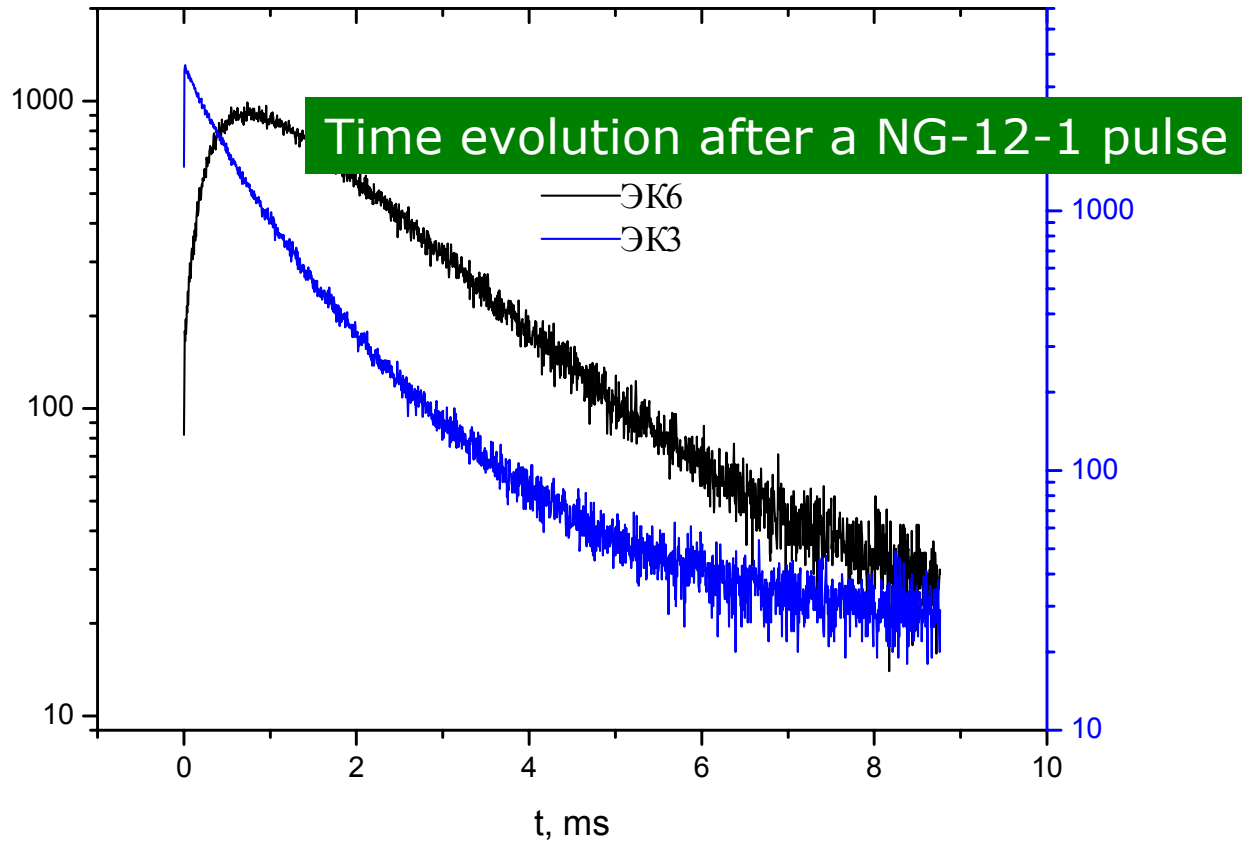
III. A comparison of experimental and calculated (MCNP-4B) results will be carried out.

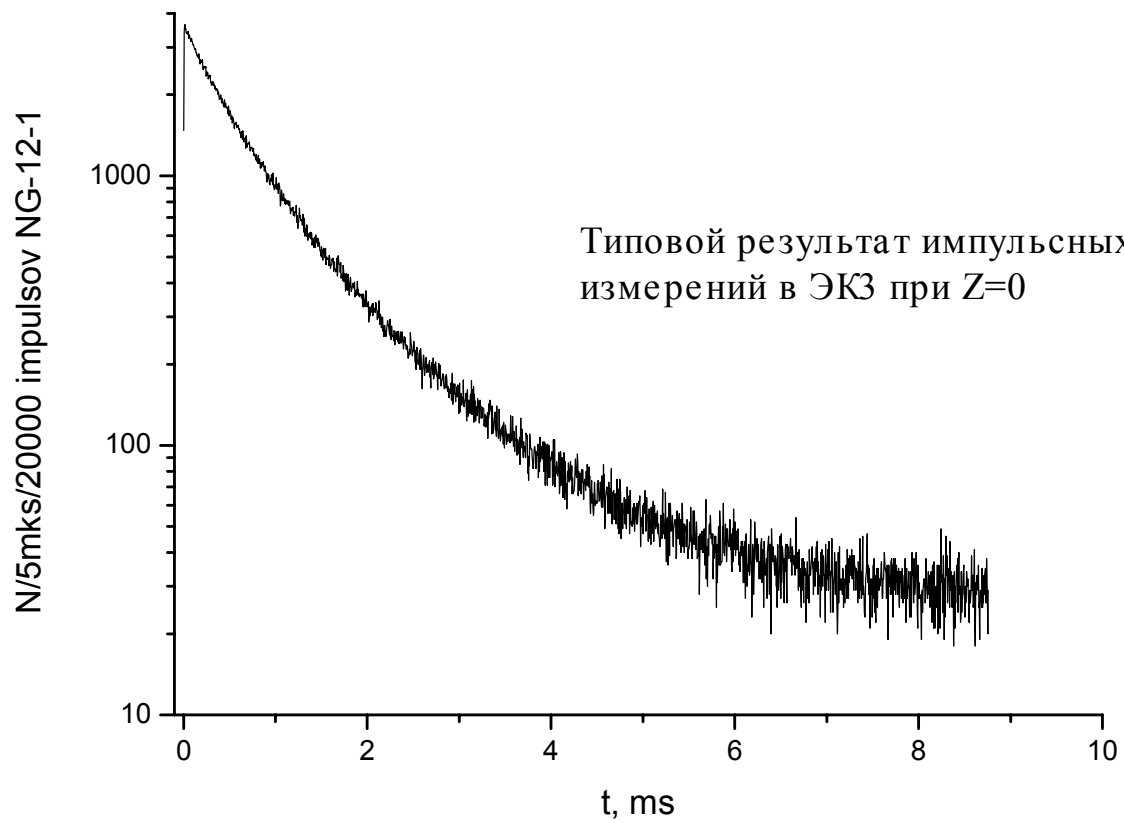
Measurements will be performed by of ^3He - detectors and fission chambers ($^{\text{U-235}}$, $^{\text{U-238}}$, $^{\text{Th-232}}$, ...) and with DT, DD and ^{252}Cf neutron sources.

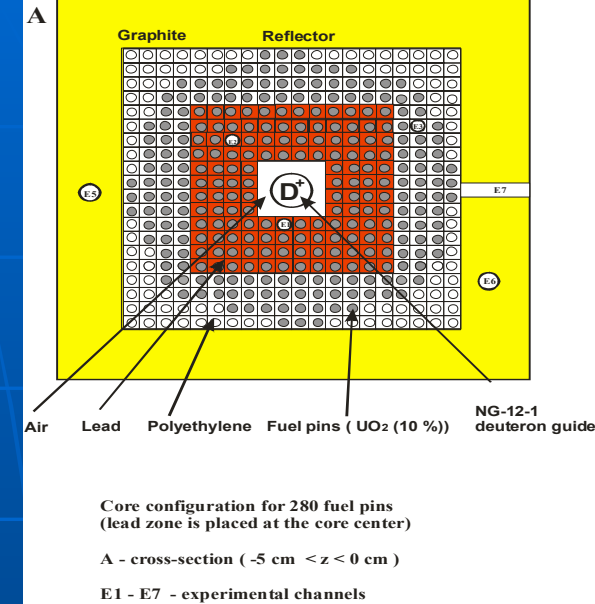
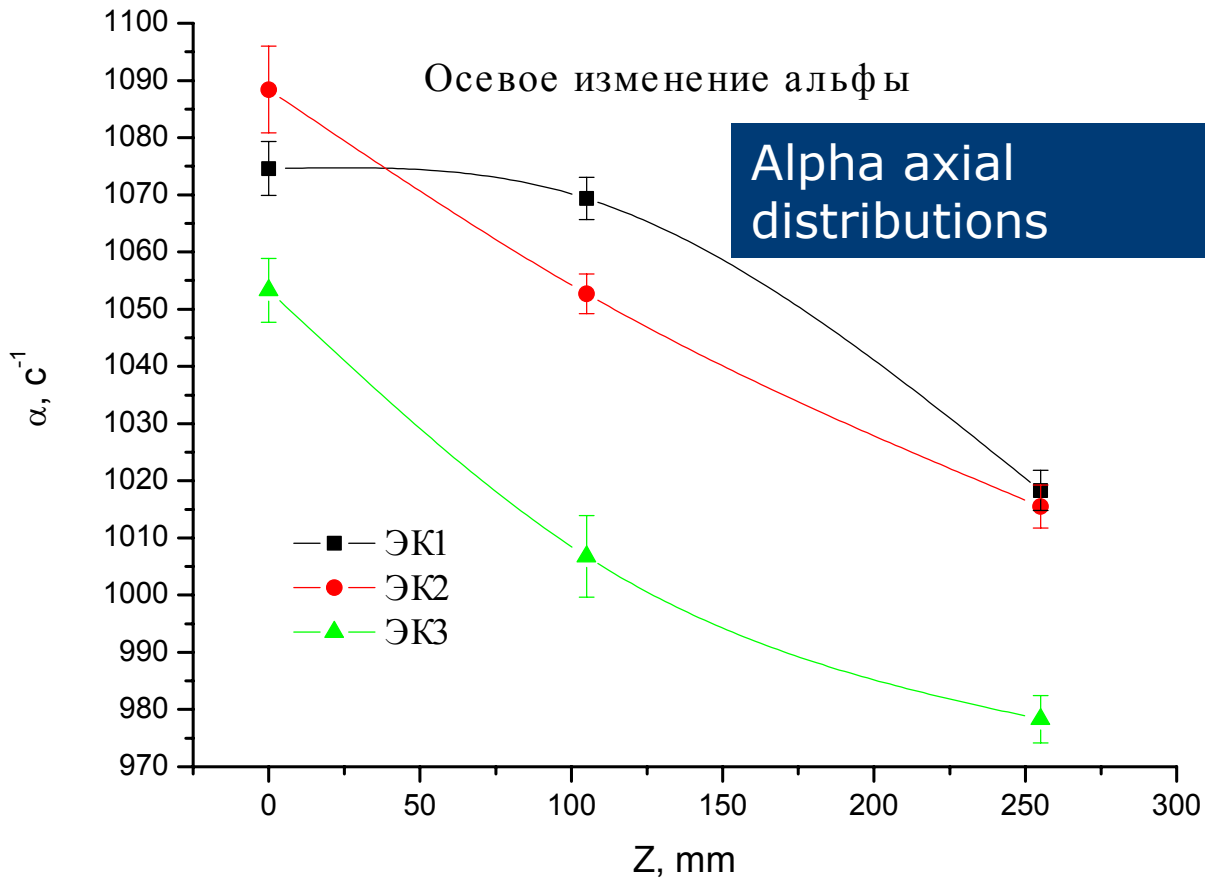
The following experimental program can be performed (?)

- 1. k_{eff} for Nrods equal to 216,245,280;
- 2. Multiplication factors k_{src} for Nrods equal to 216,245,280 with different neutron sources $S_0(E,r,z)$;
- 3. Reactivity changes $\Delta\rho$ ($\rho=(k_{eff} - 1)/ k_{eff}$) due to removal both the central and the peripheral fuel rods;
- 4. Lifetime of prompt neutrons τ_p ;
- 5. The following reaction rates inside the experimental channels: $^{129}\text{I}(n,\gamma)^{130}\text{I}$, $^{237}\text{Np}(n,\gamma)^{238}\text{Np}$, $^{243}\text{Am}(n,\gamma)^{244}\text{Am}$, $^{237}\text{Np}(n,f)$, $^{243}\text{Am}(n,f)$;
- 6. The fission reaction rates for ^{235}U inside the experimental channels;
- 7. Neutron flux densities and energy spectra as well as spectral indices $\frac{\langle\sigma f\rangle_{\text{U238}}}{\langle\sigma f\rangle_{\text{U235}}}$ and $\frac{\langle\sigma f\rangle_{\text{Th}}}{\langle\sigma f\rangle_{\text{U235}}}$, $\frac{\langle\sigma f\rangle_{\text{U233}}}{\langle\sigma f\rangle_{\text{U235}}}$, $\frac{\langle\sigma f\rangle_{\text{Pu239}}}{\langle\sigma f\rangle_{\text{U235}}}$ inside the experimental channels. Nrods equal to 216,245,280;
- ((8. External neutron source importance $\varphi^* = \langle v \rangle (1/k_{eff} - 1) \cdot P/S_0$;
- ($\varphi^* = (1 - k_{eff})/k_{eff} \cdot k_{src} / (1 - k_{src})$) for Nrods equal to 216,245,280;
- 9. Time distributions of fission rates $^{235}\text{U}(n,f)$ for Nrods equal to 216,245,280 with two neutron sources (DD,DT).

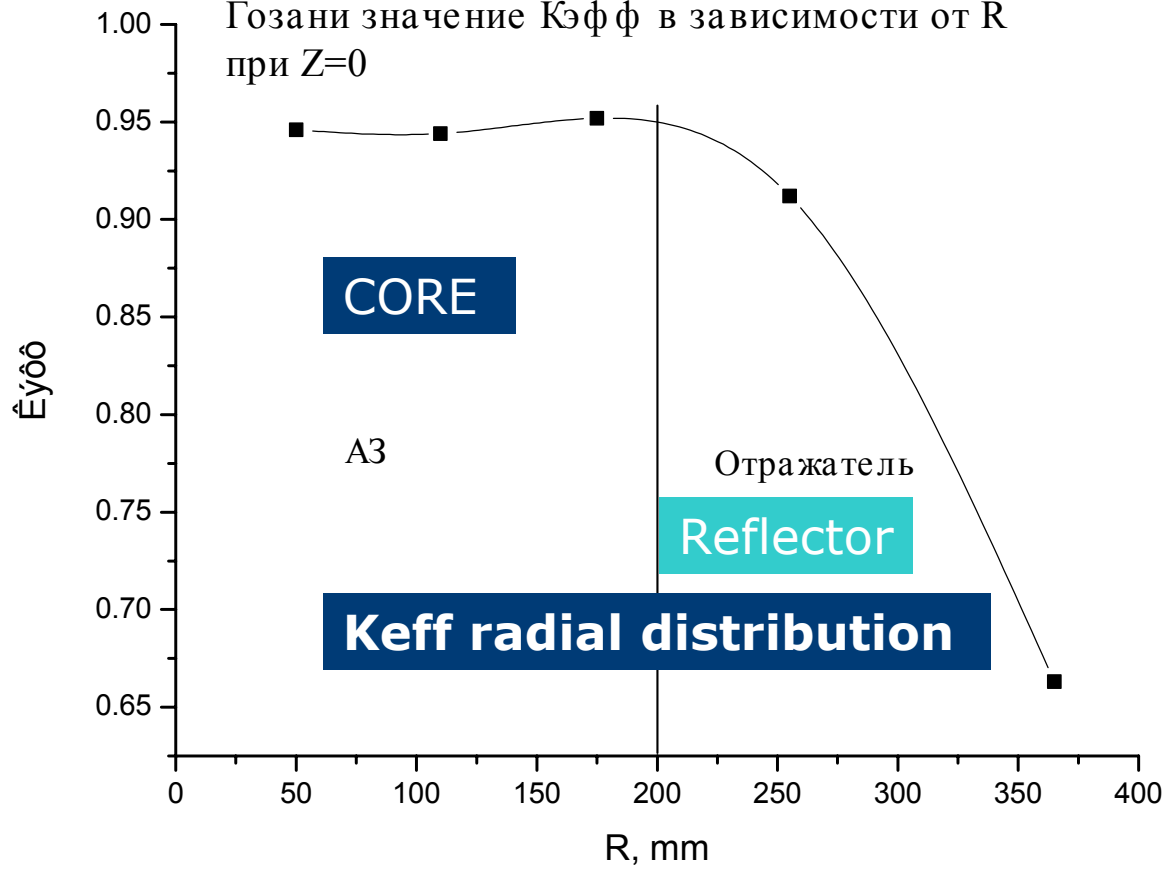
Спад плотности нейтронного потока
в АЗ - ЭКЗ и в отражателе - ЭК6

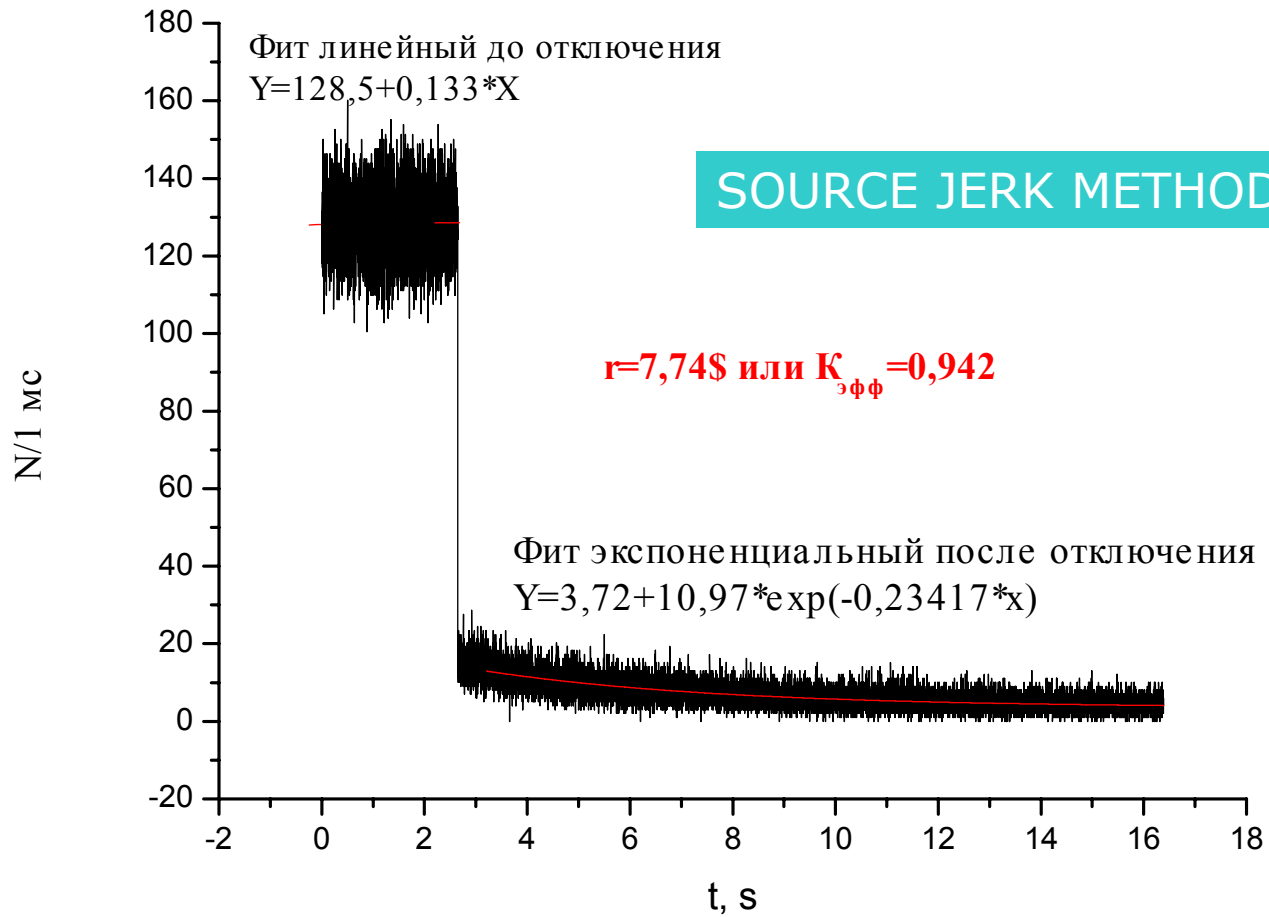






Формально рассчитанное по методу
Гозани значение $K_{эф}$ в зависимости от R
при $Z=0$





A fast spectrum booster coupled
one way to a thermal
spectrum system

It is well known that the principal difficulty of the ADS technology is the requirement of high accelerator currents. One of the promising way of solving the problem is a maximization of the neutron gain. The extra multiplication of neutrons can be achieved in the systems having central booster region having a $K_{inf} \approx 1.1$ and an outer region having K_{inf} at the level 0.97-0.98.

The main idea is to introduce source neutron in a region of high neutron importance and thereby get enhanced multiplication.

It can be achieved **in the systems with one way coupling between the two regions** - neutrons from the inner region may leak out into the outer region, however, the probability for outer region neutrons to re-enter the inner region **is to be made as low as possible.**

The practical way of achieving such a coupling between the two systems is introduction **a thermal absorber in between them.**

■ **Keff = 0,975 – 0,98**

Booster zone (Keff= 0,65):

dimension, cm 48x48x50

fuel:

Umet. is enriched to 90% in 235U

UO₂ is enriched to 36% in 235U

neutron flux density

with energy $E_n > 0,1 \text{ MeV}$, $10^9 \text{ n/(cm}^2 \text{ s)}$

moderator Pb

Uranium load (kg) U-5-62.8;U-8 - 54.5

Intermediate zone:

thickness, cm 3

material Umet (natural uranium) + B₄C

Moderator Pb

Uranium load (kg) U-5-0.23;U-8 -31.8

Thermal zone (Keff= 0,95) :

thickness, cm 24

fuel : UO₂ is enriched to 10% in 235U

moderator polyethylene

reflector

graphite

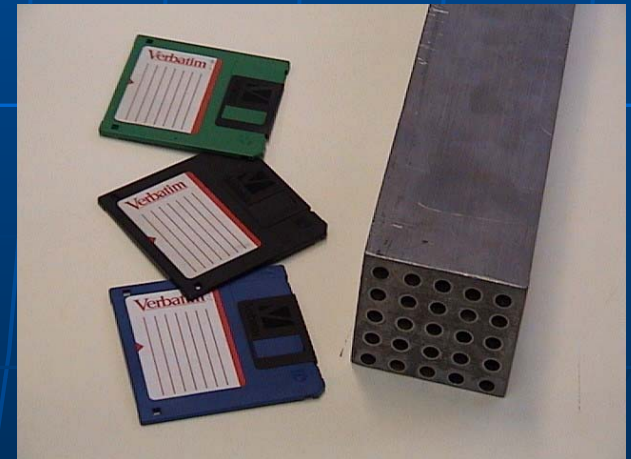
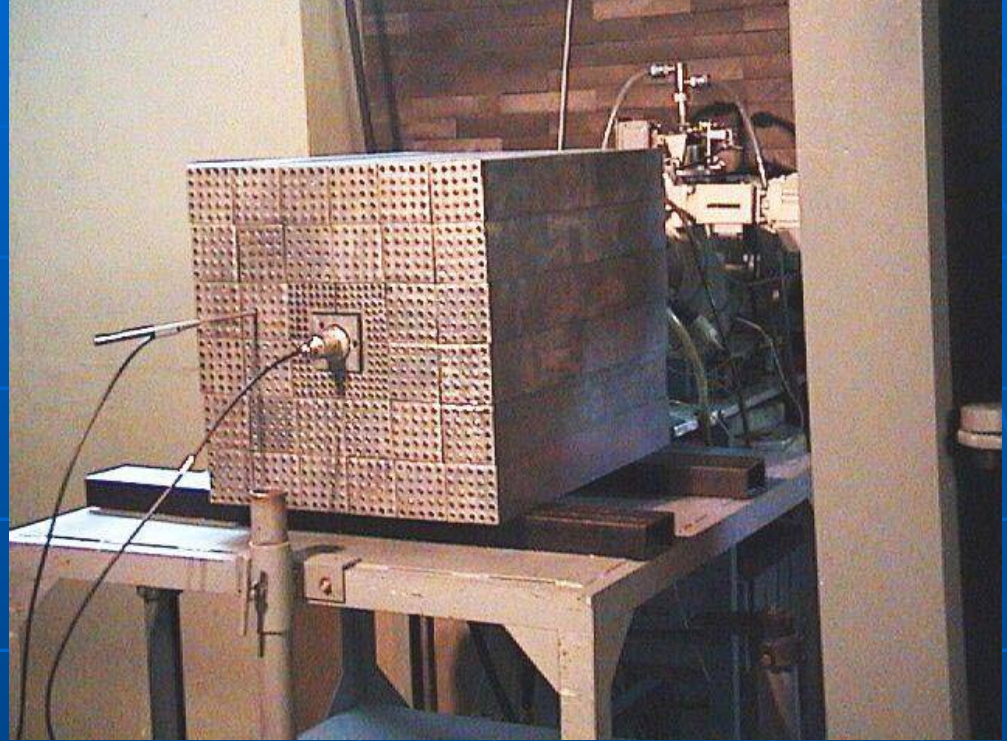
Thermal neutron flux density:

Ti³H -target $10^9 \text{ n/(cm}^2 \text{ s)}$

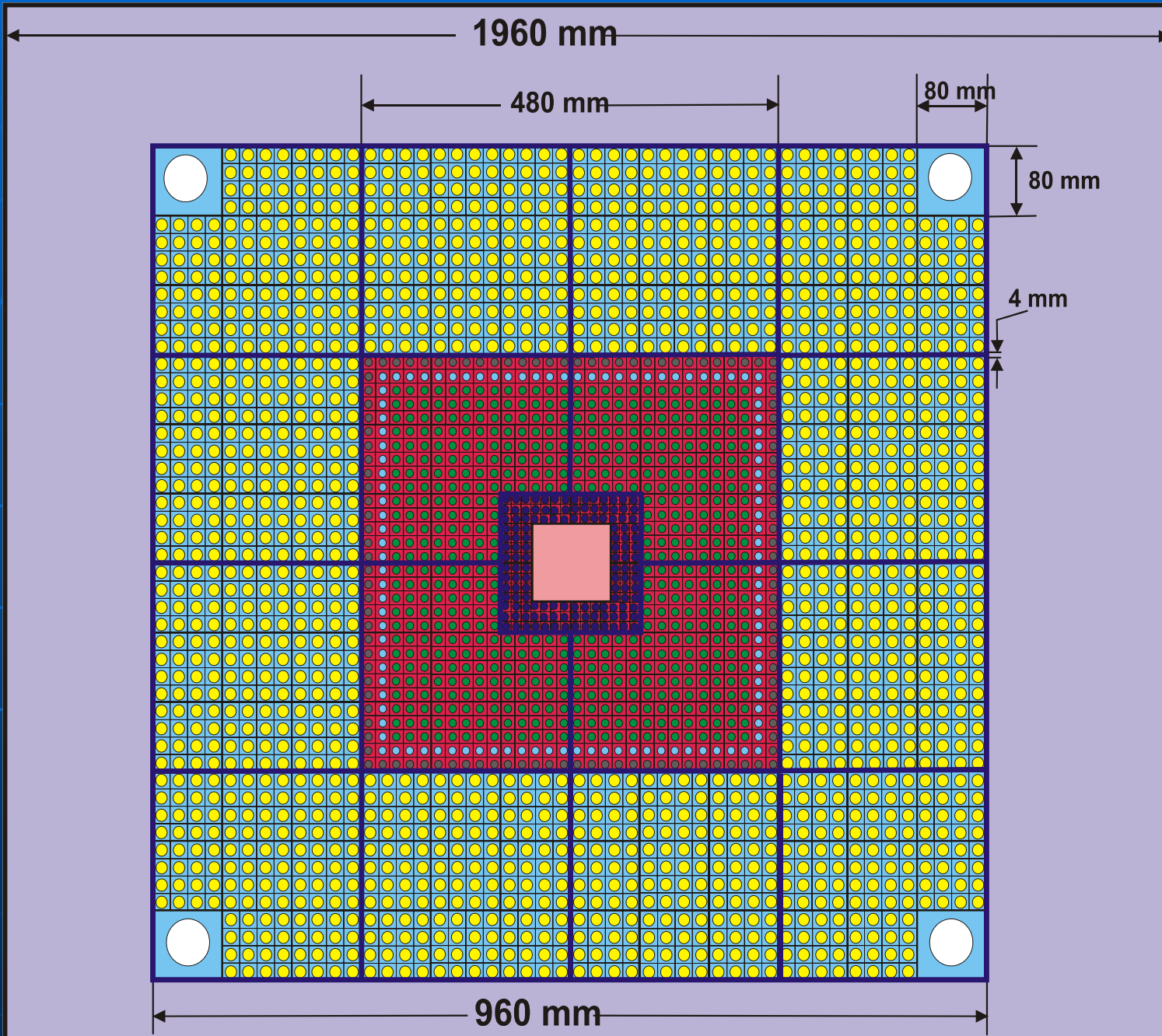
Uranium load (kg) U-5-8.07;U-8- 72.6









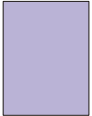
multiplication factor 50

Total uranium load (kg) U-5 -72; U-8 - 167



Booster subcritical assembly «Yalina - B», driven by a neutron generator.



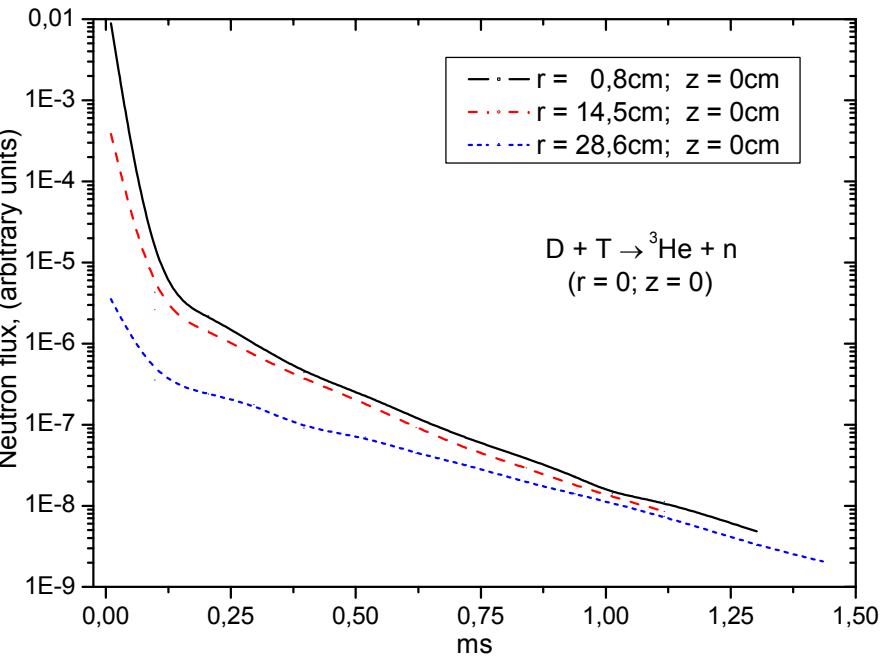
-  **Fast zone 1**
-  Umet - 90%
-  **Fast zone 2**
-  UO₂ - 36%
-  **Absorber layer**
U_{ect} - 0,7%
-  B₄C
-  **Thermal zone**
Polyethylene
-  UO₂ - 10%
-  **Graphite**

Vertical layout of booster subcritical assembly

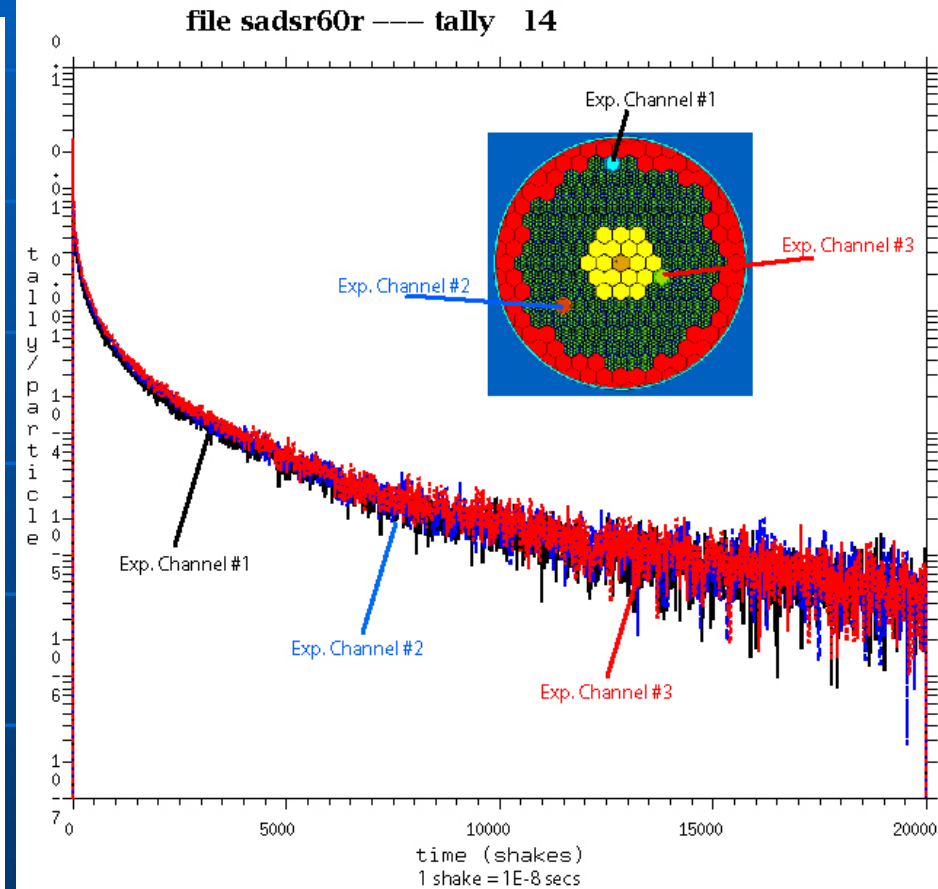


The characteristics of the fuel elements

Fast zone Fuel :	<u>90 % enriched U met.</u>		
▪	active height 50 cm ;	Fuel Cassettes	35 + 1
▪	fuel pellet		
▪	radius : 0.32 cm	Fuel elements	33
▪	Nr = 132		
▪			
▪	<u>36 % enriched UO₂</u>		
▪	active height 50 cm		
▪	fuel pellet		
▪	radius : 0.32 cm		
▪	Nr = 576		
▪			
Thermal zone	<u>10 % enriched UO₂</u>		
▪	active height 50 cm		
▪	radius : 0.45 cm		
▪	Nr = 1050		
▪	cladding: composition : stainless steel and Al thickness :		
▪	0.076cm		
▪			

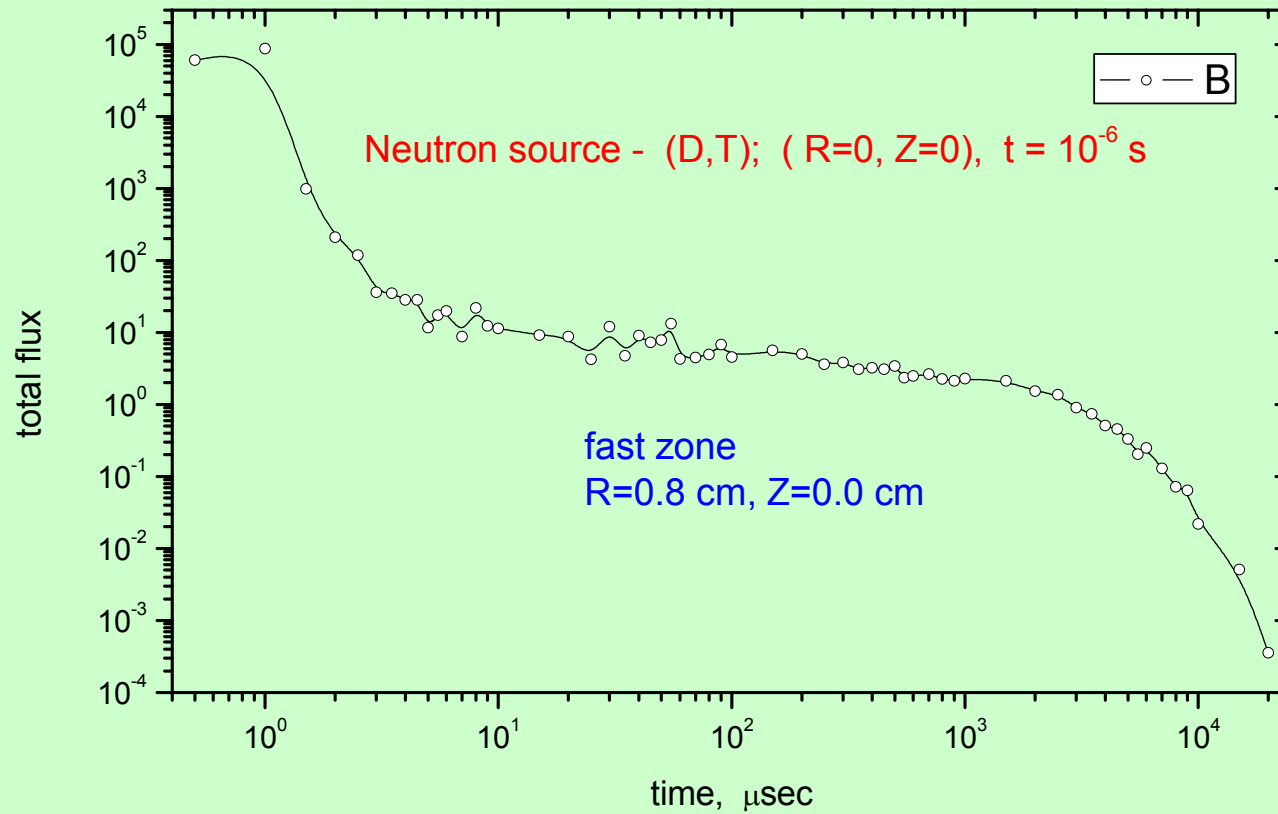


Time evolution of the neutron flux after neutron generator pulse ($\tau = 1\mu\text{s}$) at the different position (r ; z) in the core



Case #12: Time evolution of ^{235}U fission counting rate. Central height. Detectors in the 3 experimental channels at the core.

Time evolution of the neutron flux after neutron generator pulse ($\tau=1\mu\text{s}$).



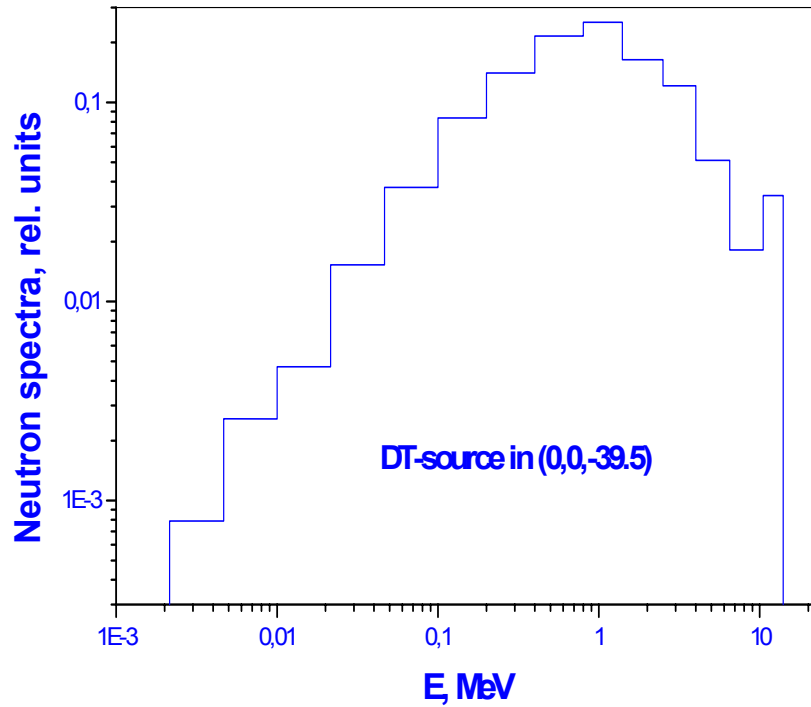
Prompt neutron lifetime in the booster subcritical assembly driven by a neutron generator

	Bare booster zone	Booster zone with polyethylene reflector	Thermal zone loaded with 1040 fuel pins	Booster subcritical assembly (thermal zone loaded with 832 fuel pins)	Booster subcritical assembly (thermal zone loaded with 448 fuel pins)	Booster subcritical assembly (full load of thermal zone - 1040 fuel pins)
Prompt neutron lifetime	5.6×10^{-8} s (0.056 μ s)	4.2×10^{-6} s (4.2 μ s) with B_4C in the intermediate zone 1.06×10^{-5} s (10.6 μ s) (without B_4C in the intermediate zone)	6.2×10^{-5} s (62 μ s)	5.52×10^{-5} s (55 μ s)	4.9×10^{-5} s (49 μ s)	5.8×10^{-5} s (58 μ s)
Neutron generation lifetime	6.6×10^{-8} s (0.066 μ s)	7.3×10^{-5} s (73 μ s) with B_4C 8.0×10^{-5} c (80 μ s) without B_4C	1.04×10^{-4} s (104 μ s)	8.4×10^{-5} s (84 μ s)	7.7×10^{-5} s (77 μ s)	9.5×10^{-5} s (95 μ s)

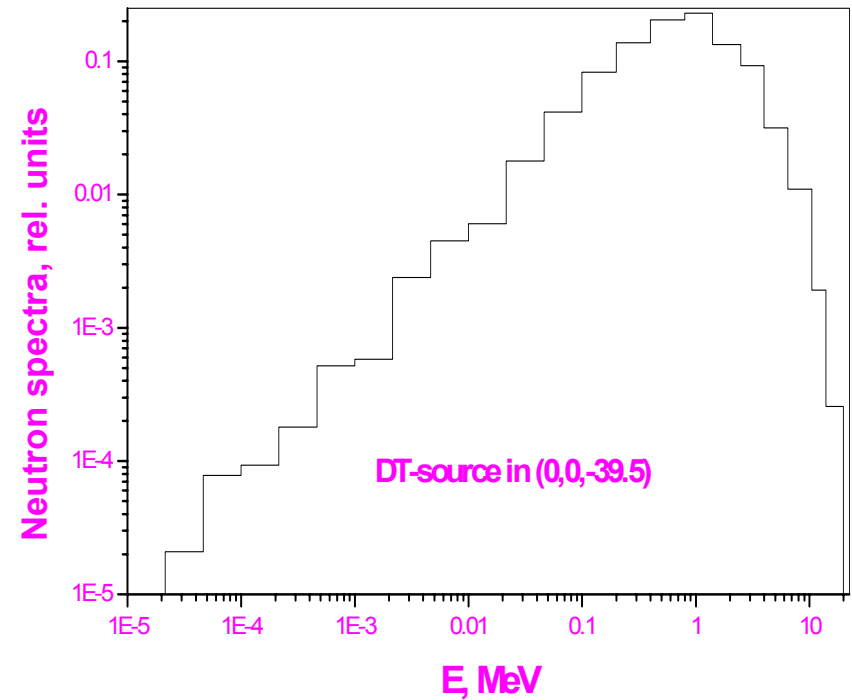
SAD A. Lopatkin $L = 24\mu$ s; E. Gonzales $L = 0.954\mu$ s ; MUSE -3 $L = 0.61 \mu$ s

Energy distribution of neutron field in the booster zone

Center of fast zone 90%U

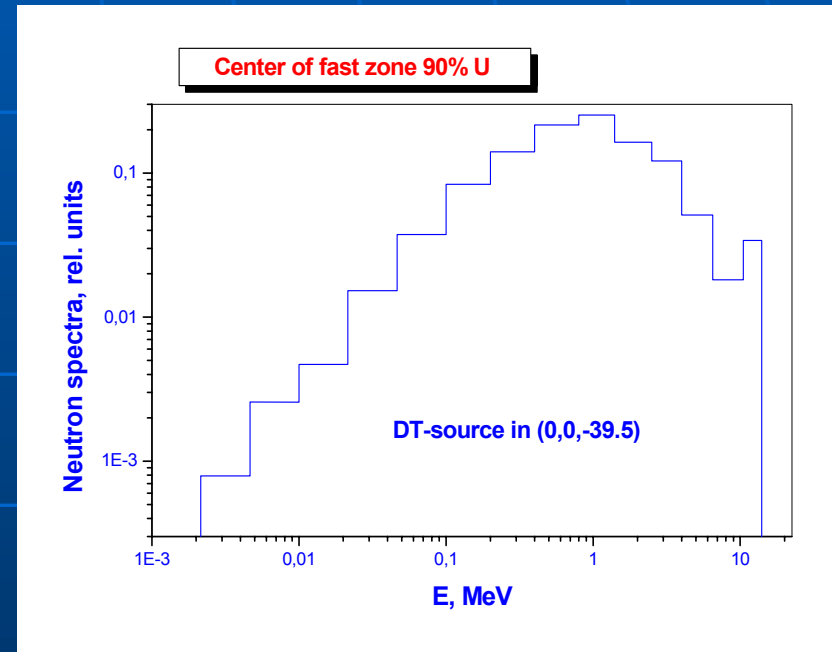
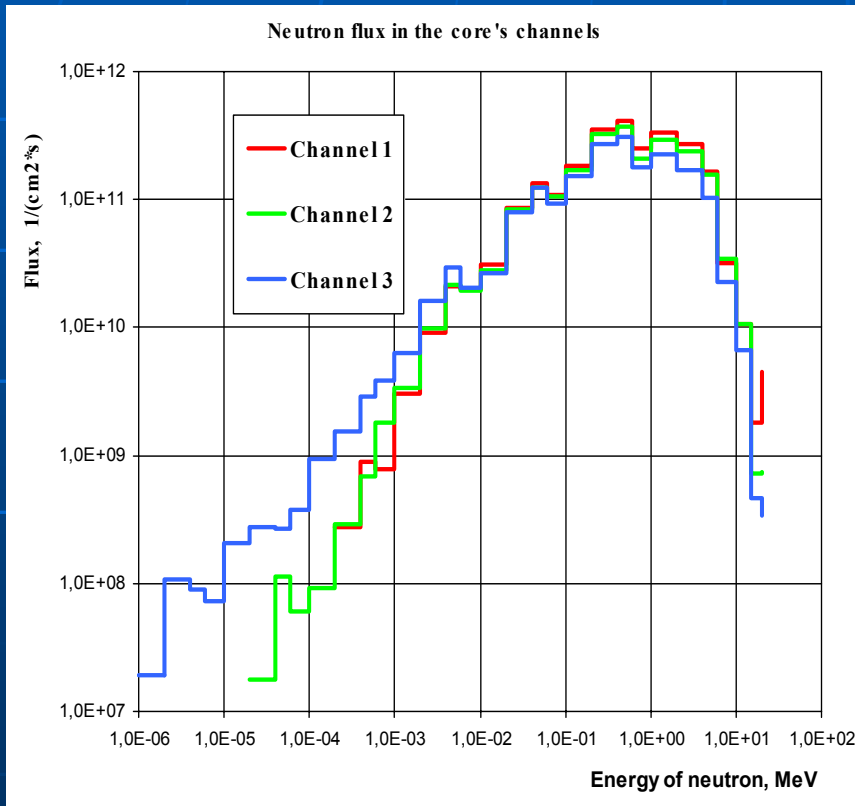


Center of fast zone 36%U



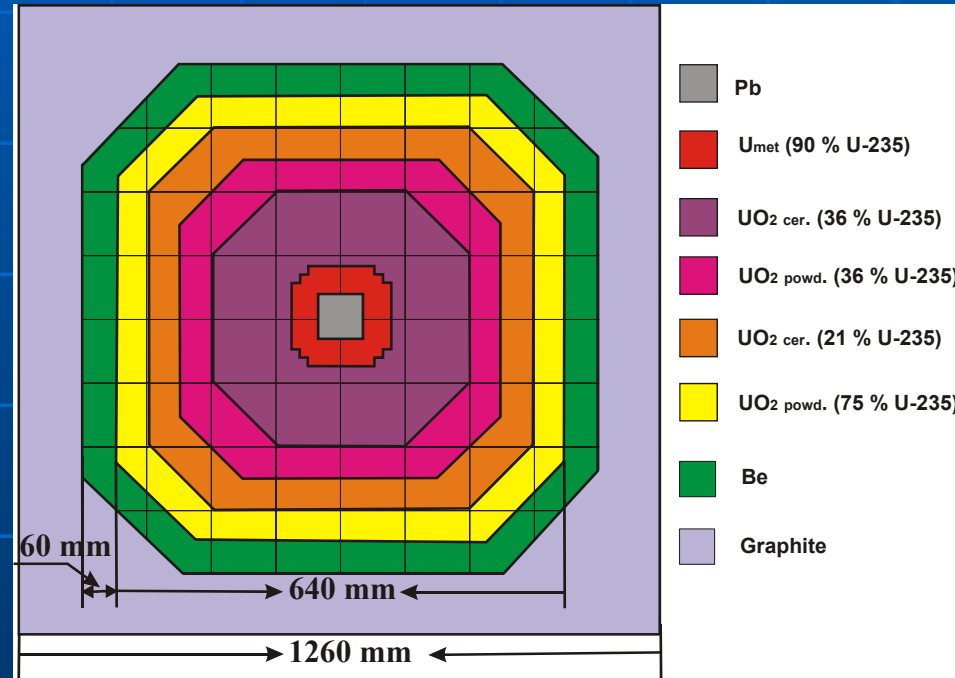
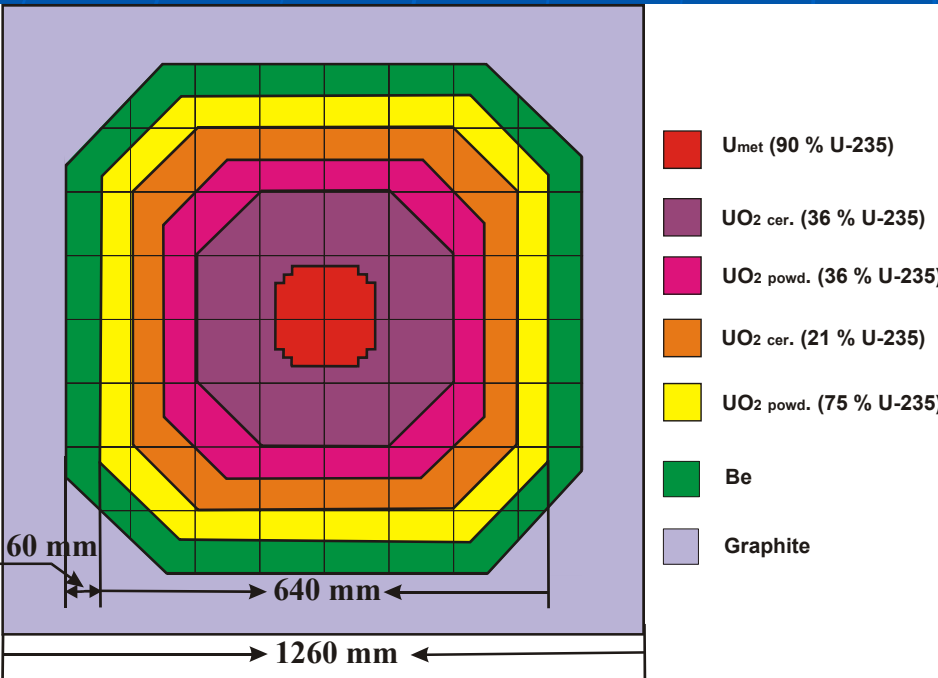
Neutron spectrum Lopatkin

Booster



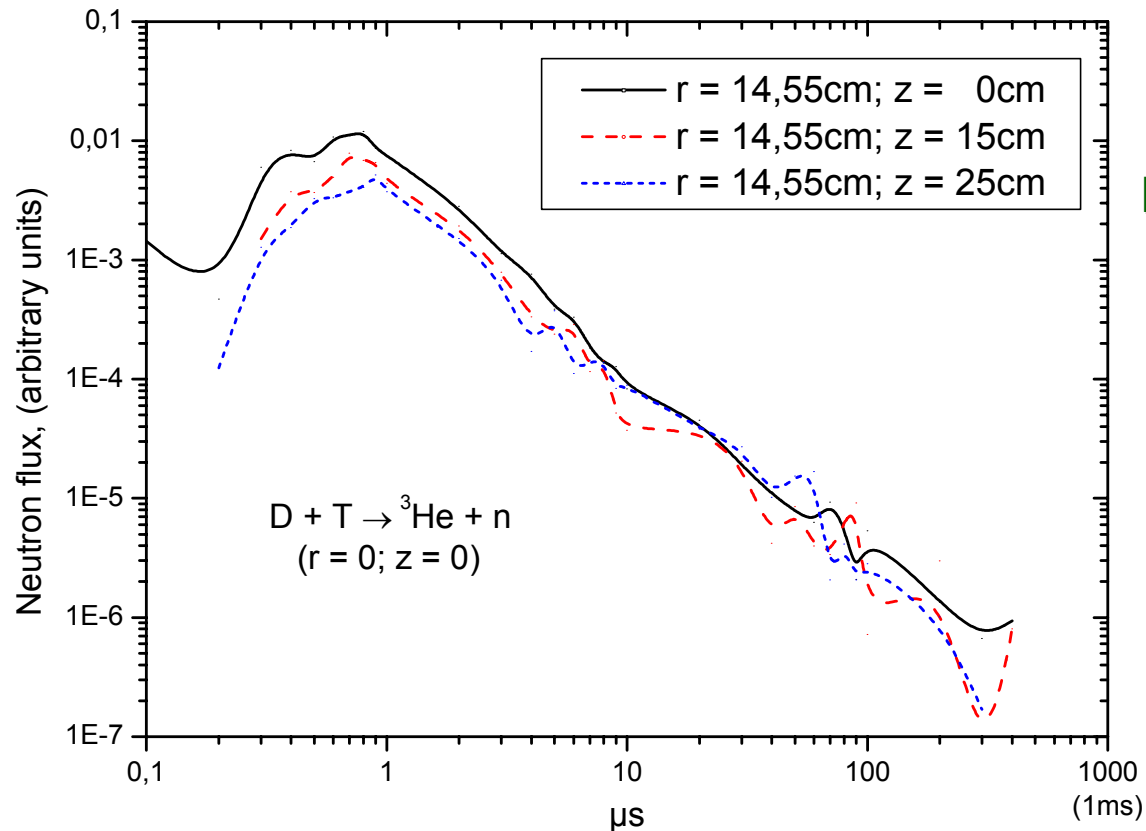
$k_{ef} = 0.93-0.95$

$k_{ef} = 0.90$



Layout (cross section) of fast neutron spectrum sub-critical assembly driven by neutron generator

($K_{eff} = 0.836$)



Bare core

Time evolution of the neutron flux after neutron generator pulse ($\tau = 1\mu\text{s}$) at the different position ($r; z$) in the core

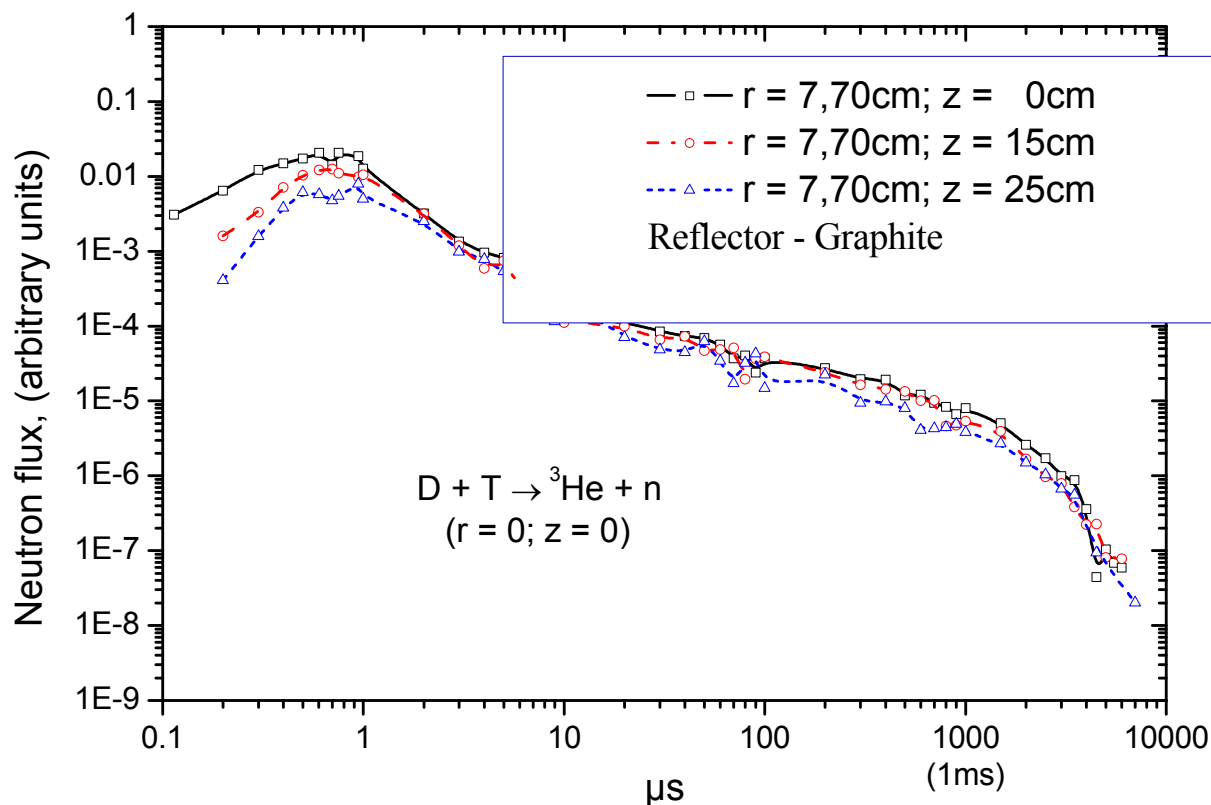
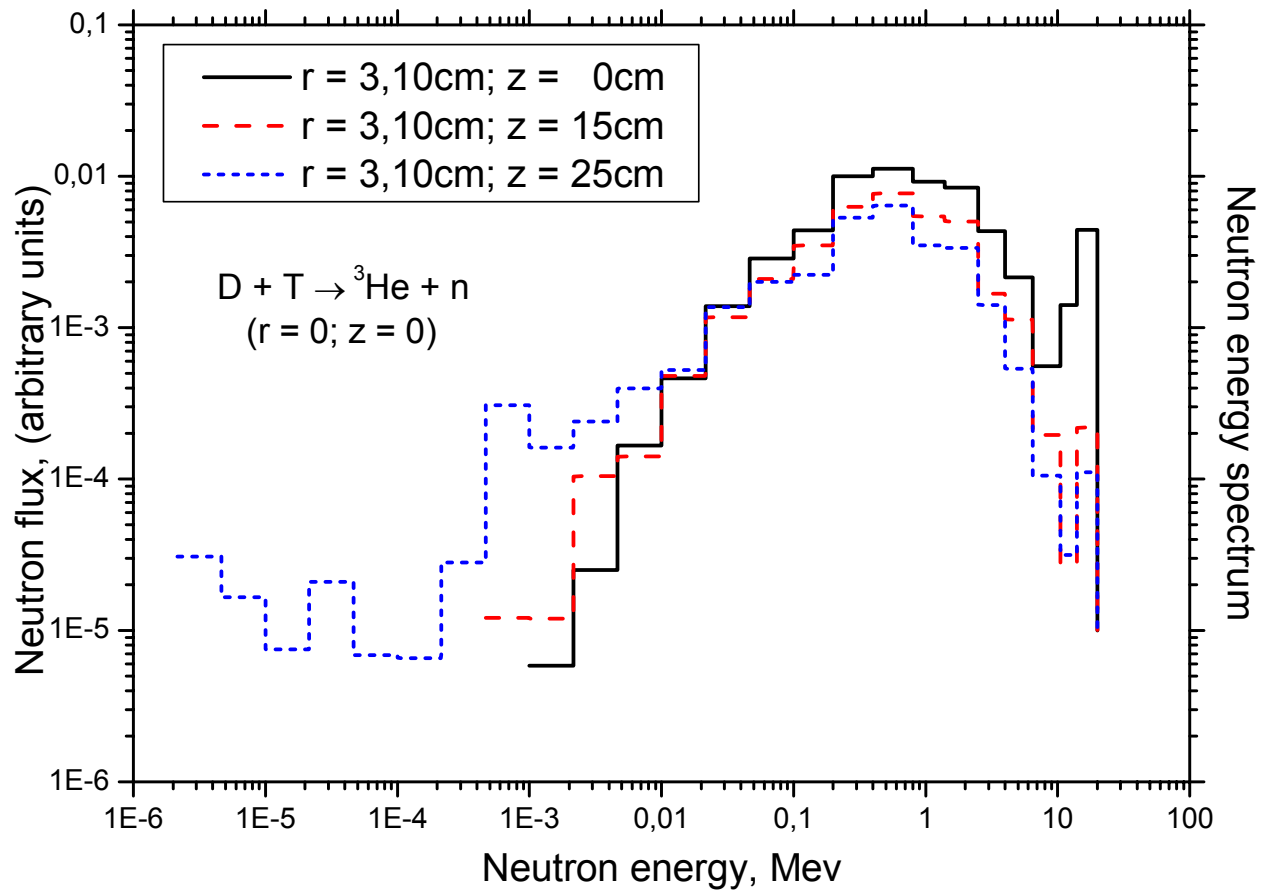


Рис. 2.2. Бустер «под SAD» с графитовым отражателем ($K_{\text{эфф}} = 0.943$).
 Временные распределения потока нейтронов в центральной части бустера ($r = 7,70$ см).



1. The booster zone of the facility YALINA-B is quite close to the SAD core (dimension, energy spectrum, time response) and from the physical point of view the some experiments dealing with neutronic of the subcritical core (SAD) can be performed on the basis YALINA-B setup. The fast zone of the facility can be considered as a volume neutron source in contrast to YALINA and MASURCA experiments. From this point of view the booster zone is closer to the spallation lead target of the SAD.
2. Measurement of the MA fission rates in the fast spectrum:
235U,237Np,238Pu,239Pu,240Pu,241Pu,242Pu,241Am,242Am
3. Studying coupling properties of the spallation target (booster zone) and reflector, blanket, shield.
4. Studying the influence of the shield on the physical parameters of the fast core.
5. Develop reactivity monitoring and techniques for subcritical systems with fast neutron spectrum
6. Validate calculation codes, libraries used to describe the subcritical core
7. The experimental determination of kinetic parameters and response to external neutron pulses.
 - Time response in different sub-critical levels

Booster research Program

- Subcriticality measurements and monitoring (K_1 , K_2 , K_{eff})
- Studying spatial and energy distributions of neutron field in subcritical cascaded system
- Measurement of the MA fission rates in the fast spectrum :
 - ^{235}U , ^{237}Np , ^{238}Pu , ^{239}Pu , ^{240}Pu , ^{241}Pu , ^{242}Pu , ^{241}Am , ^{242}Am ; and LLFP
- Studying coupling properties fast&thermal part of the core
- Measurements of the kinetic parameters cascaded system
 - (The measurement of the prompt neutron decay constant, etc,)
- Fission reaction rate for ^{235}U , ^{238}U
- Validation of code, libraries

Cross-section of the Subcritical Assembly (MOX fuel - 27% PuO_2)

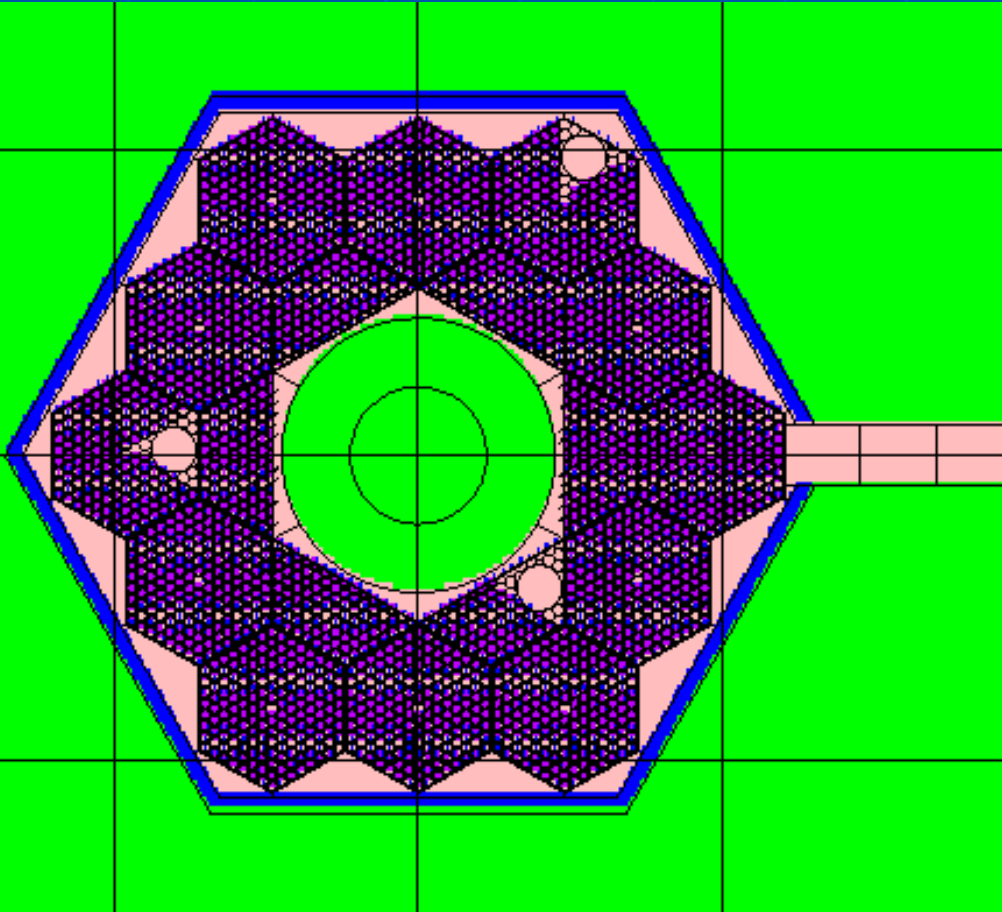
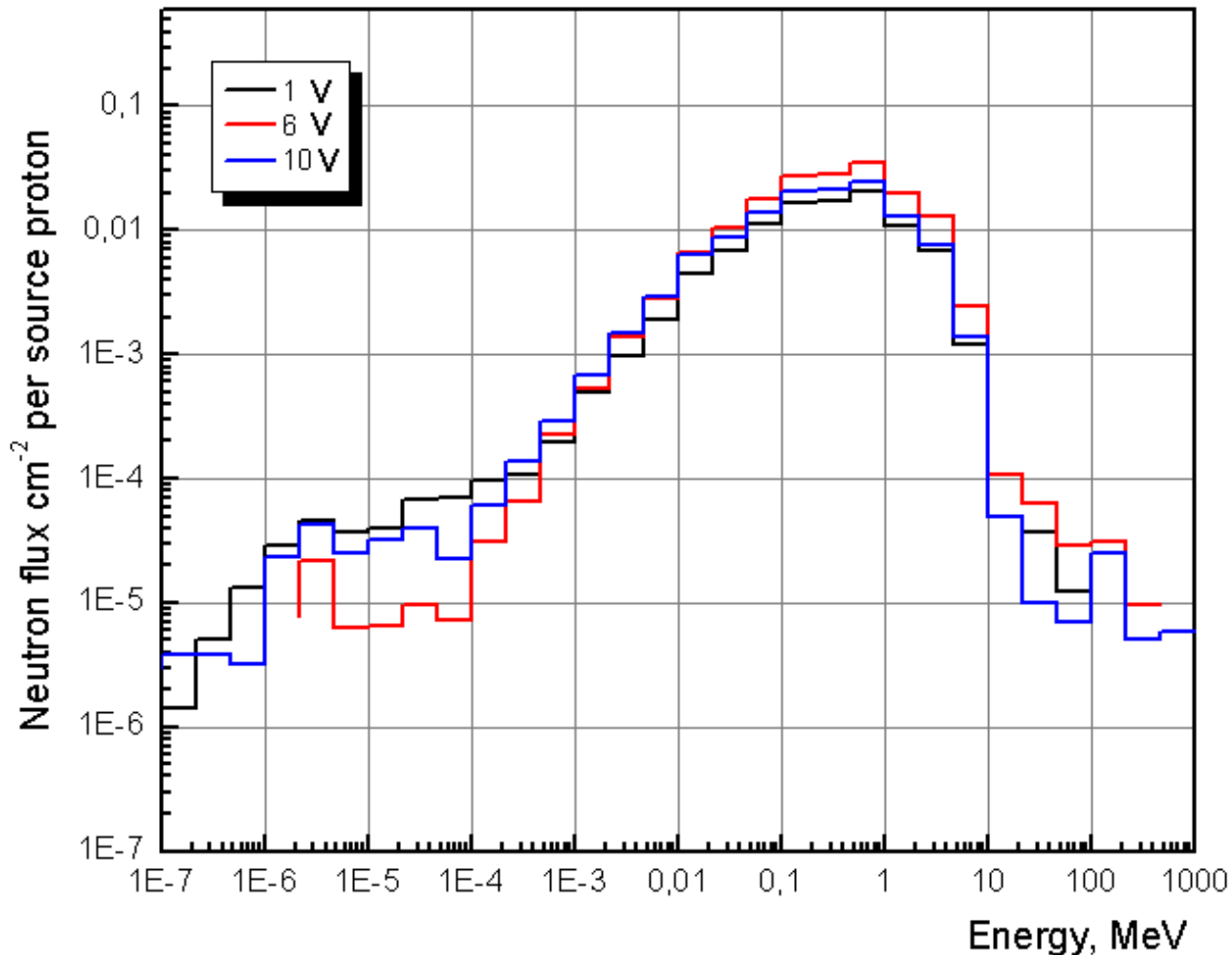


Figure shows a schematic layout of SAD-setup which has been studied in different target and reflectors. Colors symbolize different materials: yellow – lead or tungsten target, light blue – air, dark violet – MOX-fuel, green – lead, orange-lead or beryllium reflector, blue–steel.

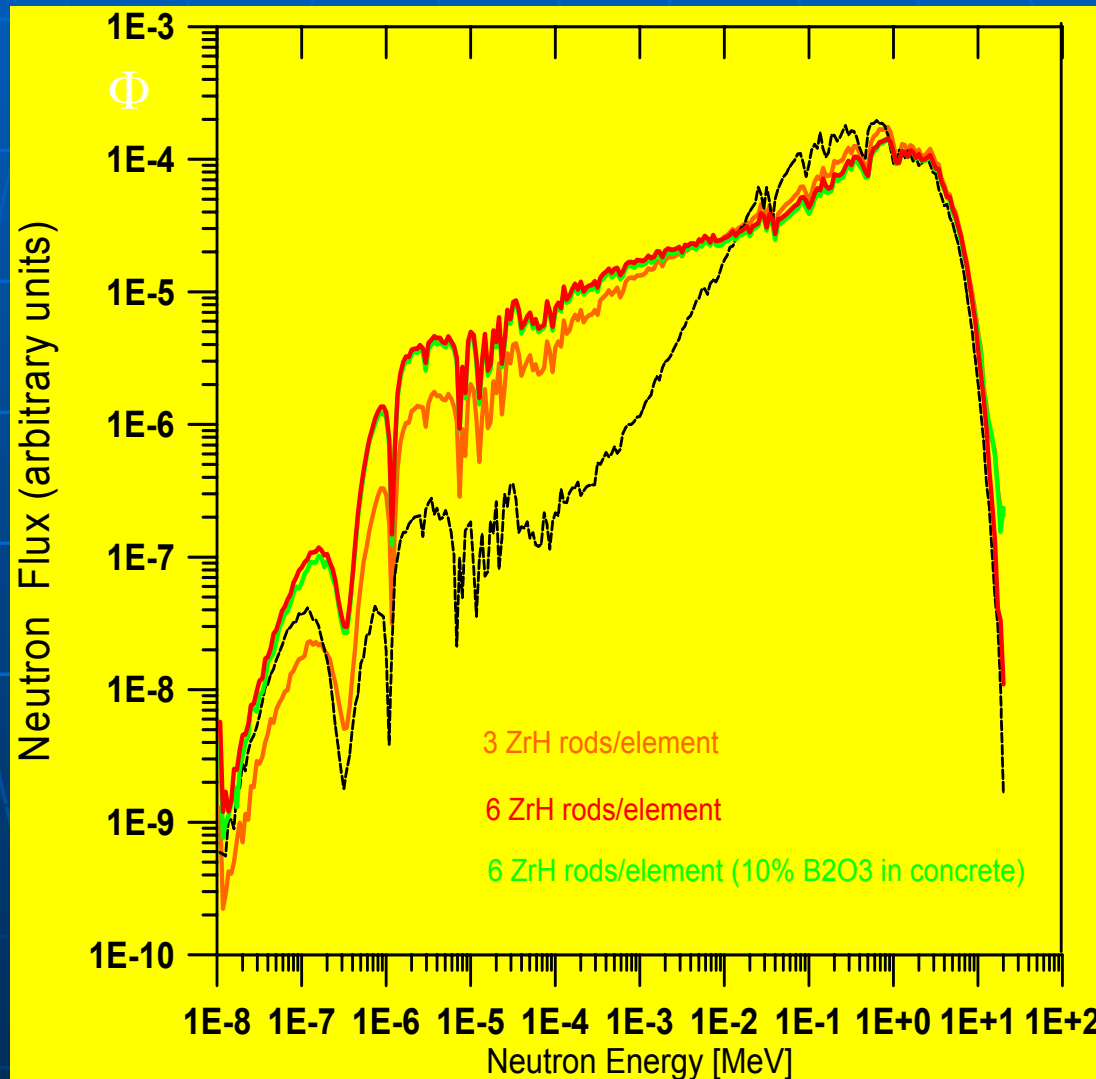
Neutron spectra calculated for the subcritical assembly.

Vertical experimental chanal in the middle of the AC. (No 2)



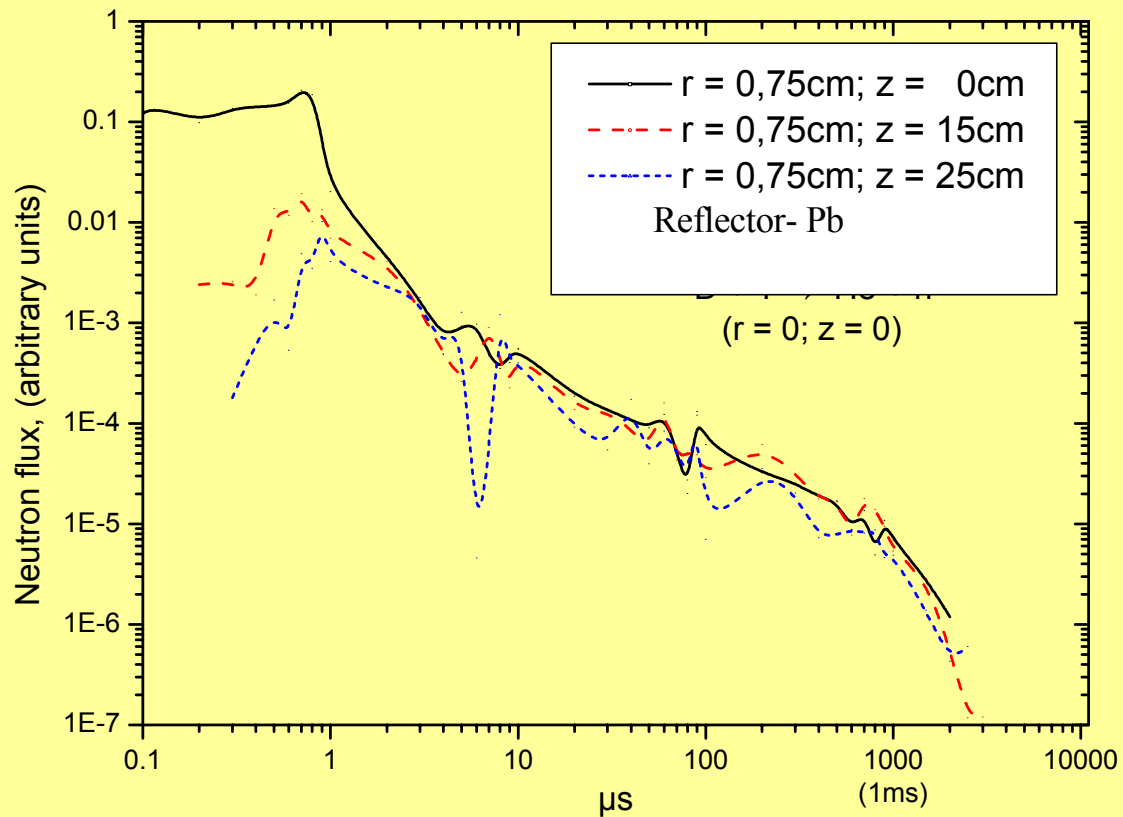
Modelling of SAD experiments

Neutron Spectra in SAD models

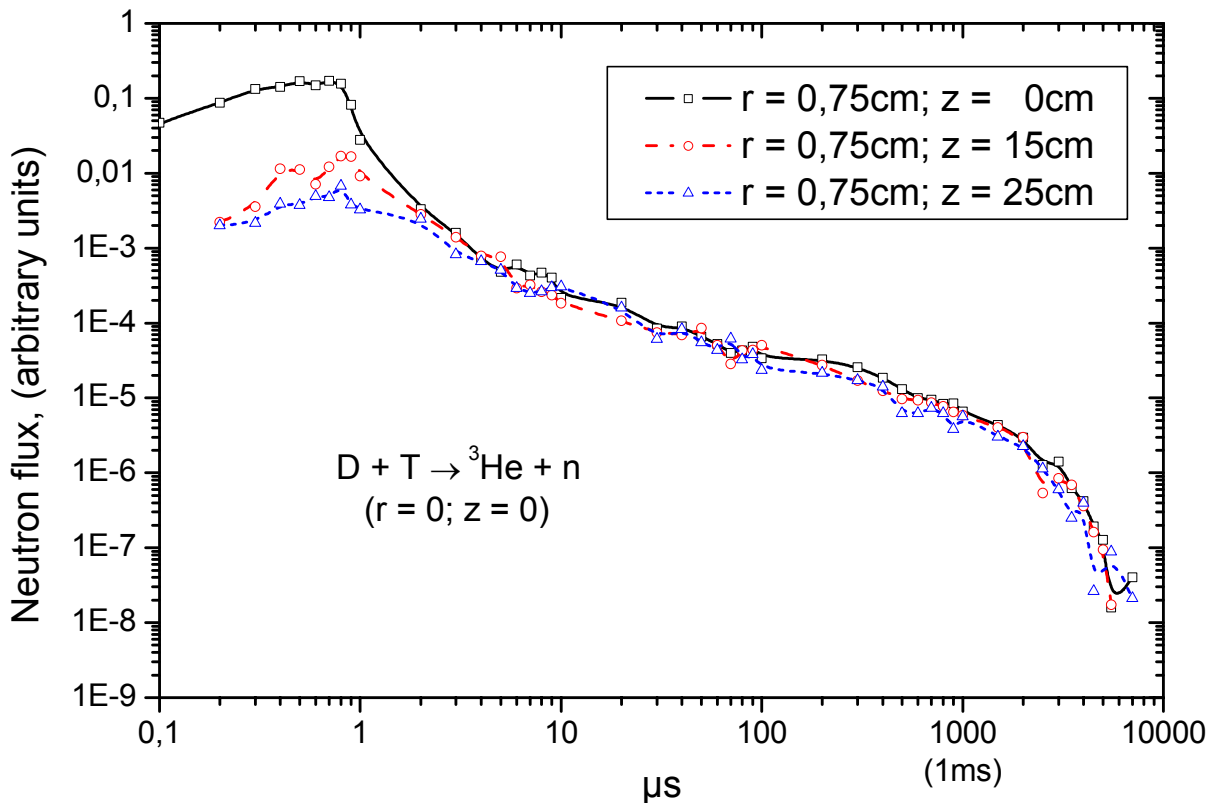


ZrH moderated options

As compared with unmoderated options, ZrH heightens the flux in the resonance region, whereas much less in the thermal region.



Time evolution of the neutron flux after neutron generator pulse ($\tau = 1\mu\text{s}$) at the different position (r; z) in the core



Time evolution of the neutron flux after neutron generator pulse ($\tau = 1\mu\text{s}$) at the different position ($r; z$) in the core

Рис. 2.1. Бустер «под SAD» с графитовым отражателем

($K_{\text{eff}} = 0.943$). Временные распределения потока нейтронов в центре сборки ($r = 0,75$ см),